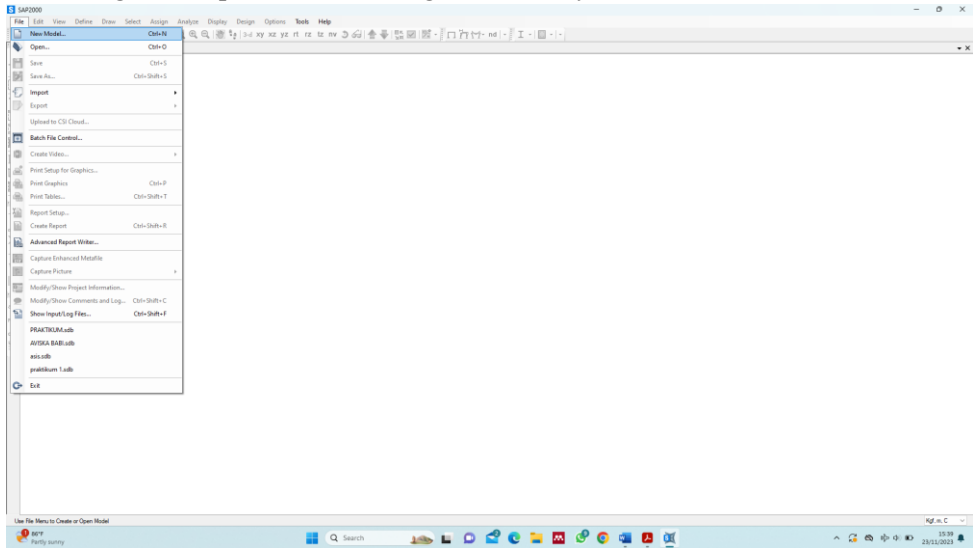


# LAMPIRAN I

## PERMODELAN STRUKTUR MENGGUNAKAN SAP2000

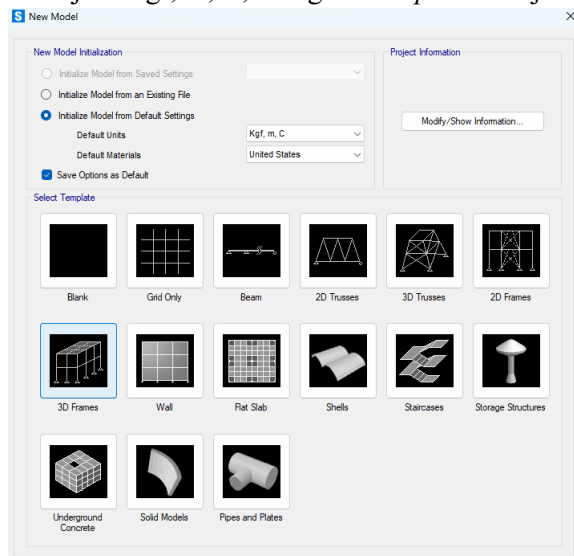
### Langkah-1: Pembuatan Model Bangunan

Pada tahap permodelan SAP2000 v.22.0.0, langkah awal yaitu membuat permodelan sesuai dengan data perencanaan, dengan cara klik *file – new model*.



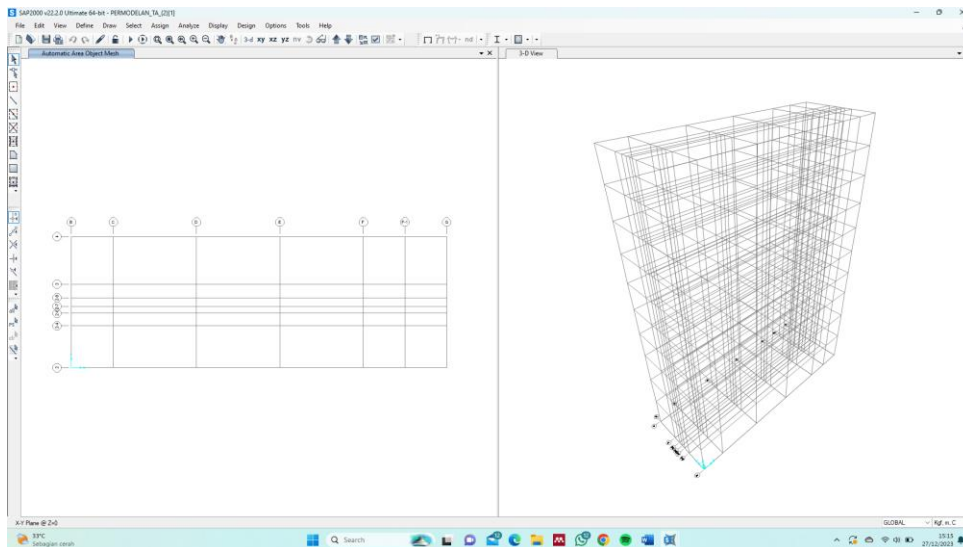
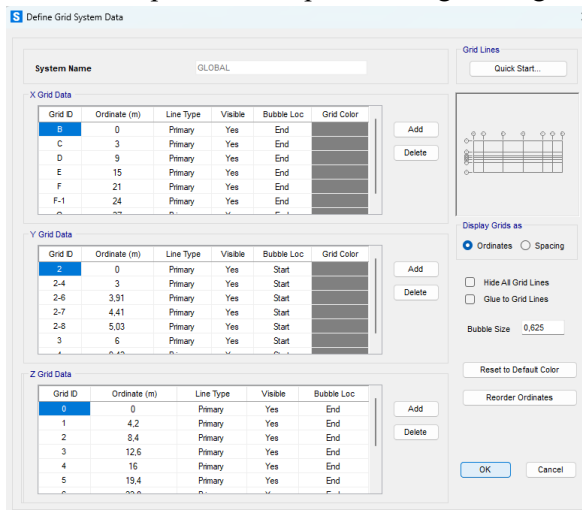
### Langkah-2: Ubah Satuan dan Template

Ubah satuan menjadi Kgf, m, C, lalu ganti *template* menjadi *3D Frames*.



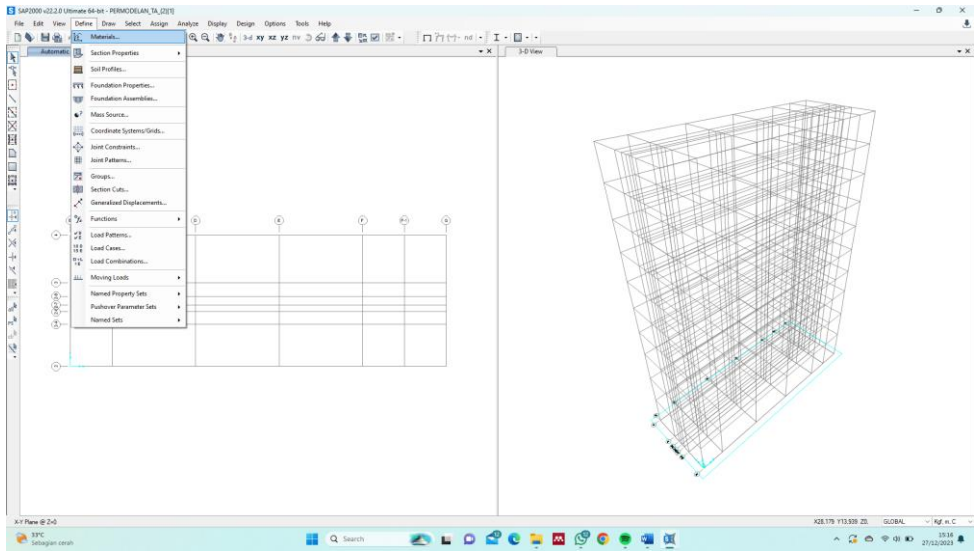
### **Langkah-3: Menentukan Ukuran Permodelan**

Setelah memilih *template* menjadi *3D Frames*, lalu klik *Modify/Show Information – Checklist "Use Custome Grid Spacing and Locate Origin"* – *edit grid*. Lalu tentukan ukuran permodelan sesuai data perencanaan pada masing-masing arah *x*, *y*, dan *z*.

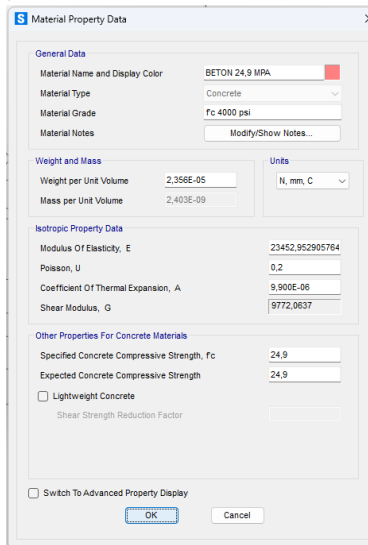


### **Langkah-4: Menentukan Material yang digunakan**

Langkah selanjutnya yaitu menentukan jenis material yang digunakan dengan cara klik *Define – Materials – Add New Materials – Modify/Show Material*.



(Spesifikasi material beton)



(Spesifikasi material baja tulangan polos)

**Material Property Data**

**General Data**

Material Name and Display Color: UL\_POLOS 240 MPA (BJTP 24)

Material Type: Rebar

Material Grade: Grade 60

Material Notes:

**Weight and Mass**

Weight per Unit Volume: 7,697E-05

Mass per Unit Volume: 7,849E-09

Units: N, mm, C

**Uniaxial Property Data**

Modulus Of Elasticity, E: 200000

Poisson, U: 0,3

Coefficient Of Thermal Expansion, A: 1,170E-05

Shear Modulus, G: 78903,07

**Other Properties For Rebar Materials**

Minimum Yield Stress, Fy: 240

Minimum Tensile Stress, Fu: 390

Expected Yield Stress, Fye: 360

Expected Tensile Stress, Fue: 585

Switch To Advanced Property Display

(Spesifikasi material baja tulangan ulir)

**Material Property Data**

**General Data**

Material Name and Display Color: TUL\_ULIR 400 MPA (BJTD 40)

Material Type: Rebar

Material Grade: Grade 60

Material Notes:

**Weight and Mass**

Weight per Unit Volume: 7,697E-05

Mass per Unit Volume: 7,849E-09

Units: N, mm, C

**Uniaxial Property Data**

Modulus Of Elasticity, E: 200000

Poisson, U: 0,3

Coefficient Of Thermal Expansion, A: 1,170E-05

Shear Modulus, G: 78903,07

**Other Properties For Rebar Materials**

Minimum Yield Stress, Fy: 400

Minimum Tensile Stress, Fu: 500

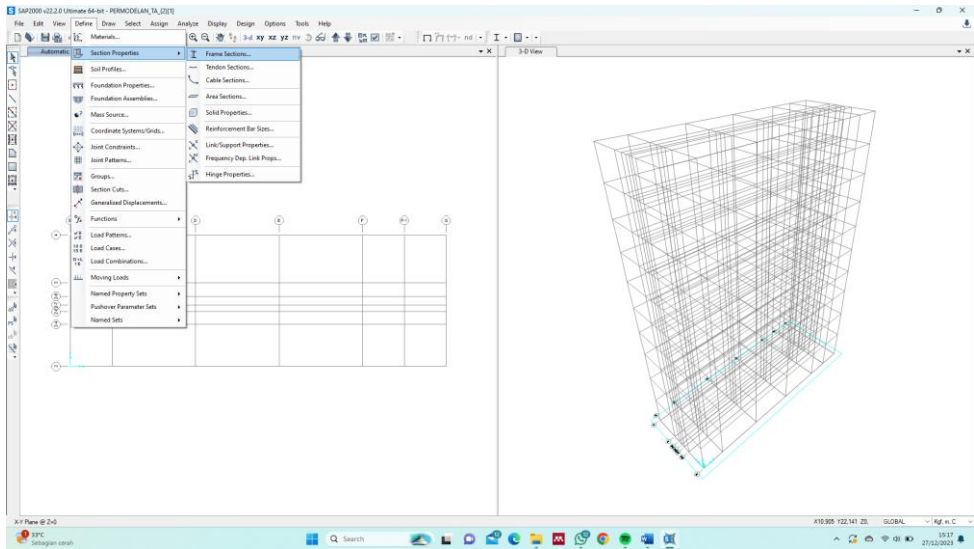
Expected Yield Stress, Fye: 600

Expected Tensile Stress, Fue: 750

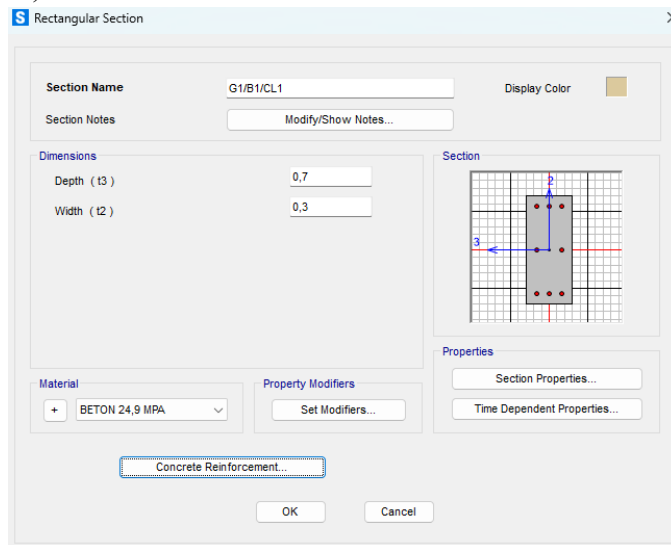
Switch To Advanced Property Display

### **Langkah-5: Memasukkan Dimensi Balok dan Kolom**

Masukkan dimensi balok dan kolom dengan cara klik *Define – Section Properties – Frame Sections – Add New Property – Concrete – Rectangular*.



(Dimensi Balok)



Klik *Reinforcement Data* dan ubah sesuai data perencanaan.

**S Reinforcement Data** [X]

**Rebar Material**

Longitudinal Bars + TUL. ULIR 400 MPA (BJT v)

Confinement Bars (Ties) + TUL. POLOS 240 MPA (f v)

**Design Type**

Column (P-M2-M3 Design)

Beam (M3 Design Only)

**Concrete Cover to Longitudinal Rebar Center**

Top 0,15

Bottom 0,15

**Reinforcement Overrides for Ductile Beams**

	Left	Right
Top	0,	0,
Bottom	0,	0,

OK Cancel

Klik *Set Modifiers* dan ubah sesuai data perencanaan

**S Rectangular Section** [X]

Section Name G1/B1/CL1 Display Color [Pink]

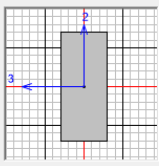
Section Notes Modify/Show Notes...

**Dimensions**

Depth (t3) 0,7

Width (t2) 0,3

**Section**



**Material** + BETON 24,9 MPA v

**Property Modifiers** Set Modifiers...

Concrete Reinforcement...

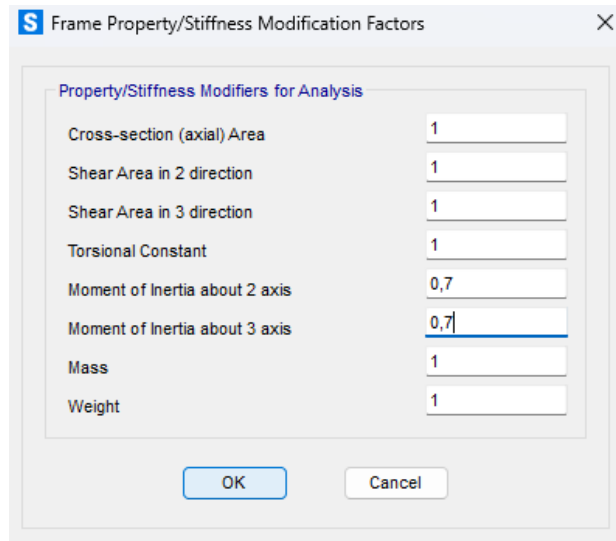
Section Properties... Time Dependent Properties...

OK Cancel

(Dimensi Kolom)

Klik *Reinforcement Data* dan ubah sesuai data perencanaan.

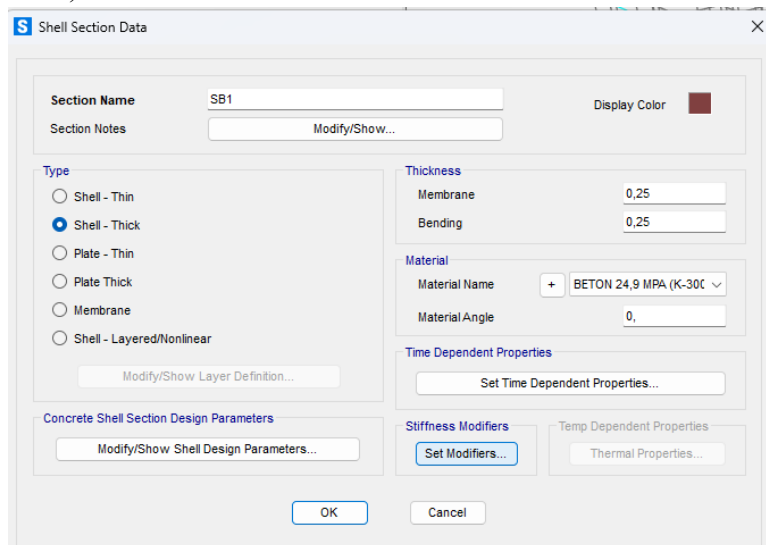
Klik *Set Modifiers* dan ubah sesuai data perencanaan



### **Langkah-6: Memasukkan Dimensi Pelat dan Shearwall**

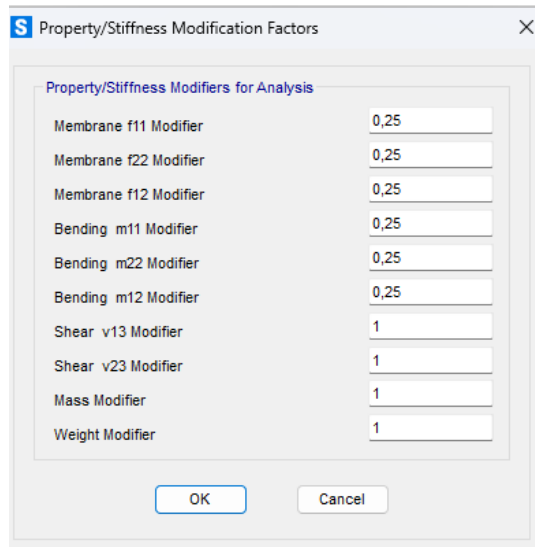
Masukkan dimensi pelat dan *shearwall* dengan cara klik *Define – Section Properties – Area Sections – Add New Property – Shell*.

(Dimensi Pelat)

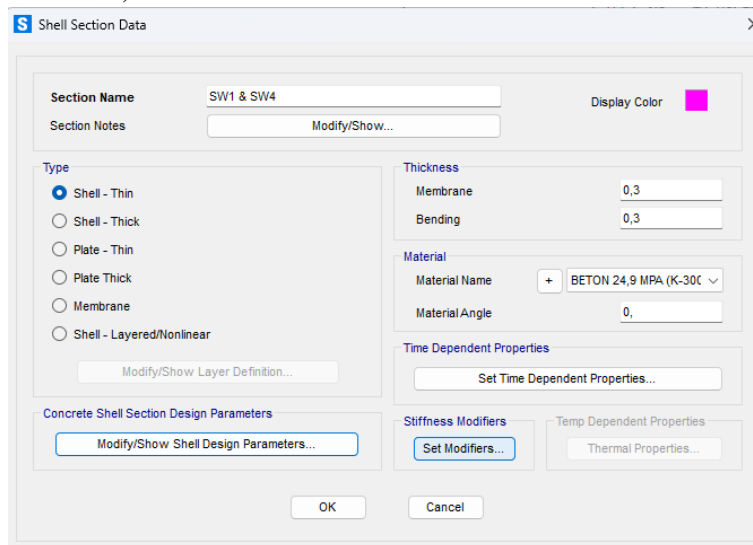


Klik *Set Modifiers* dan ubah sesuai data perencanaan



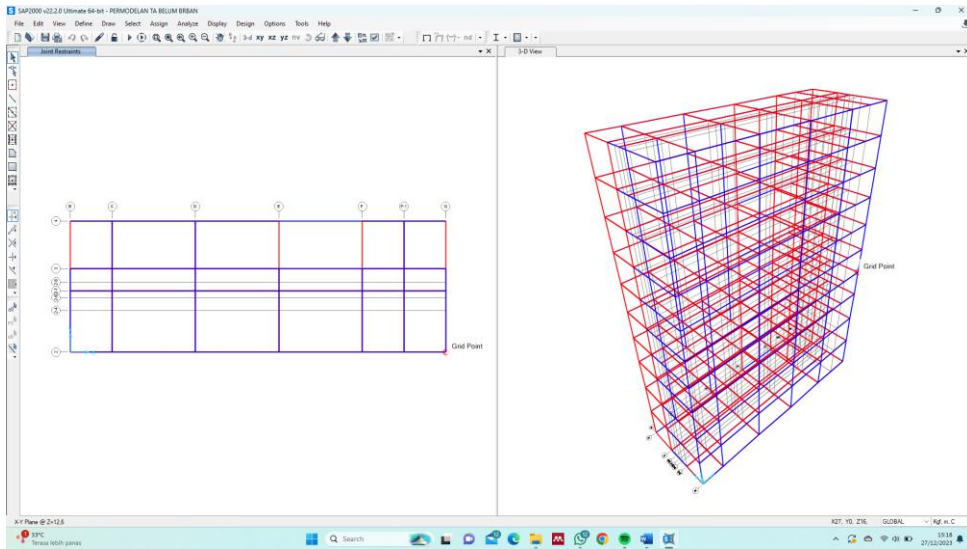


(Dimensi *Shearwall*)

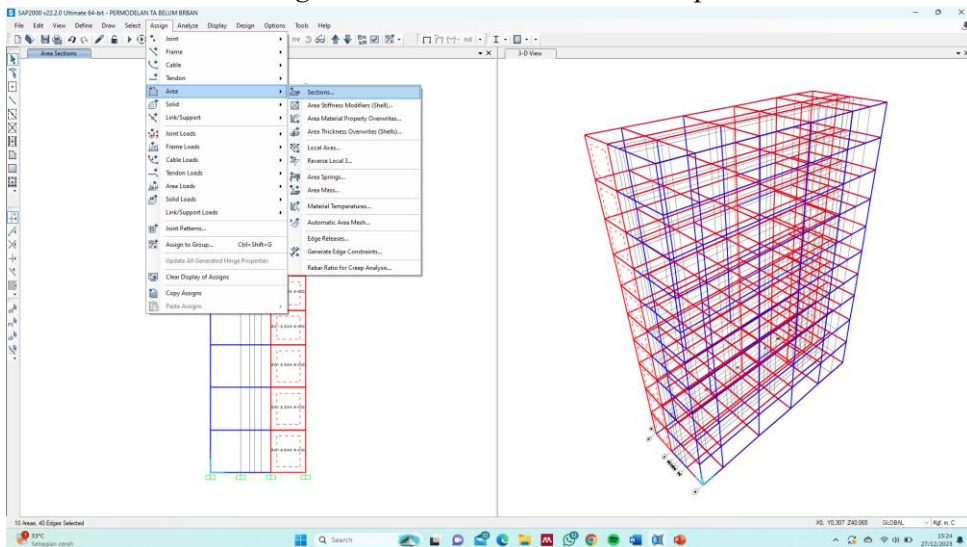


### **Langkah-7: Membuat Balok, Kolom, dan Pelat**

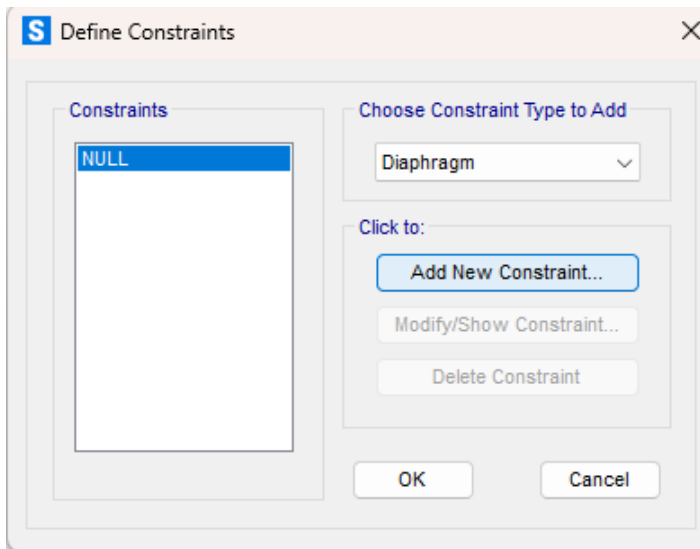
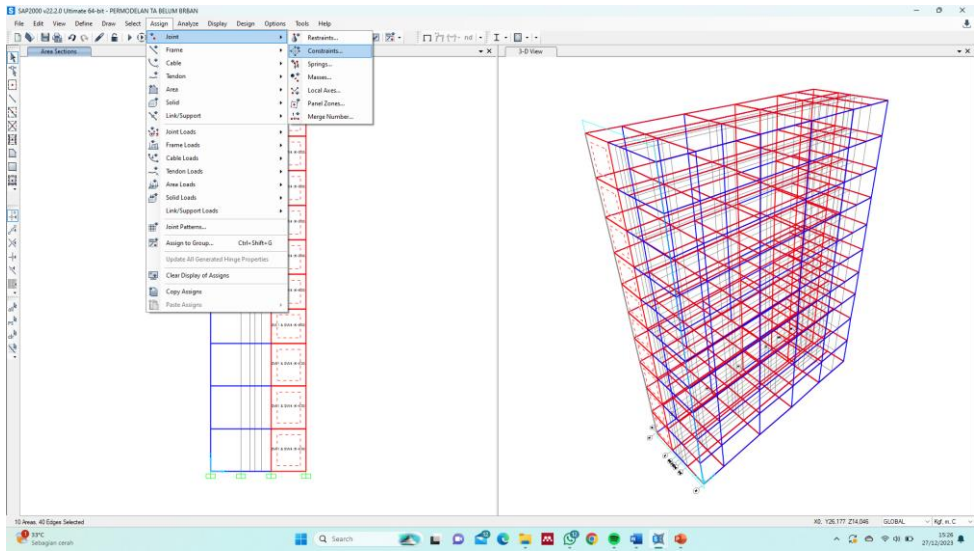
Langkah selanjutnya yaitu menggambar balok, kolom, dan pelat pada grid yang telah dibuat dengan cara klik *Draw – Draw Frame* (untuk kolom) – *Quick Draw Frame* (untuk balok) – *Draw Rectangular Area* (untuk pelat).

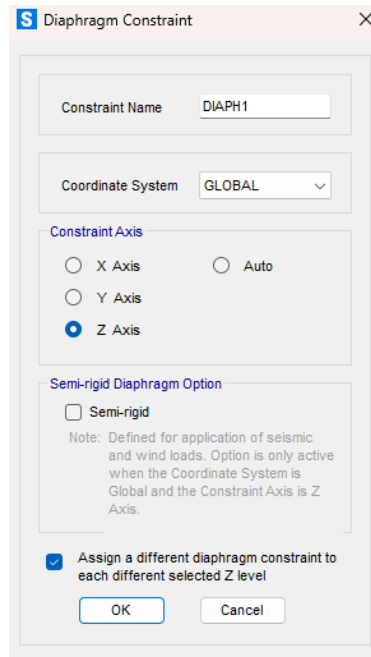


Untuk *shearwall* klik *Assign – Area – Sections – Shearwall* pada area *shearwall*.

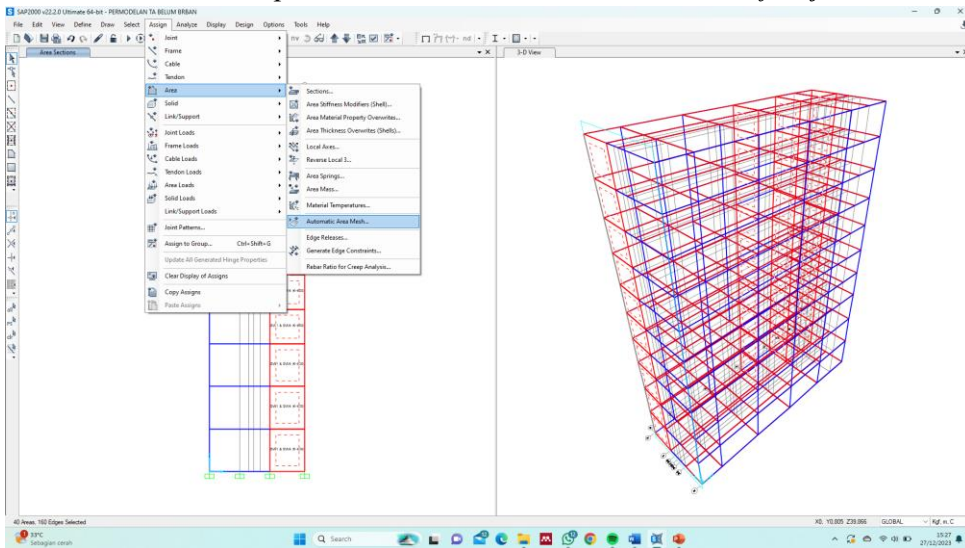


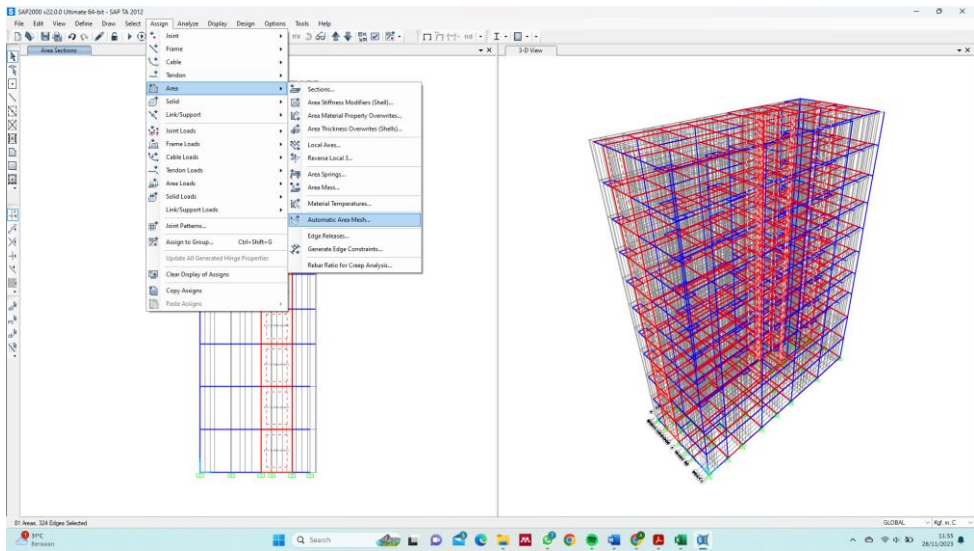
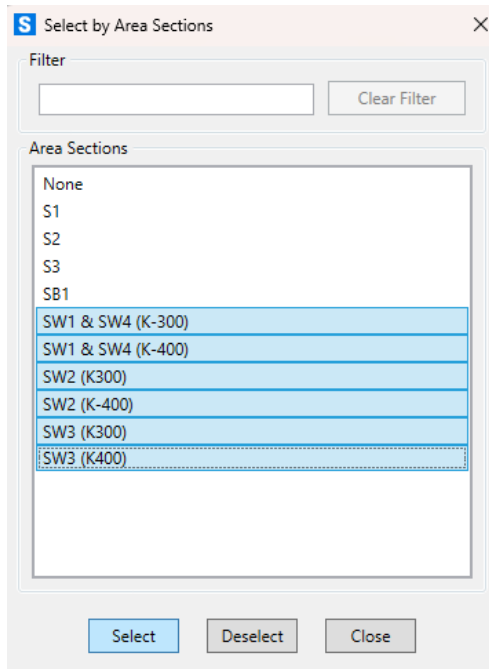
Blok area *shearwall*, lalu klik *Assign – Joint – Constraint – Define – Joint Constraint – Constraint Type* diganti menjadi *Diaphragm – Add New Constraint – Checklist “Assign Different Diaphragm Constraint to each Different Selected Z Level”*.

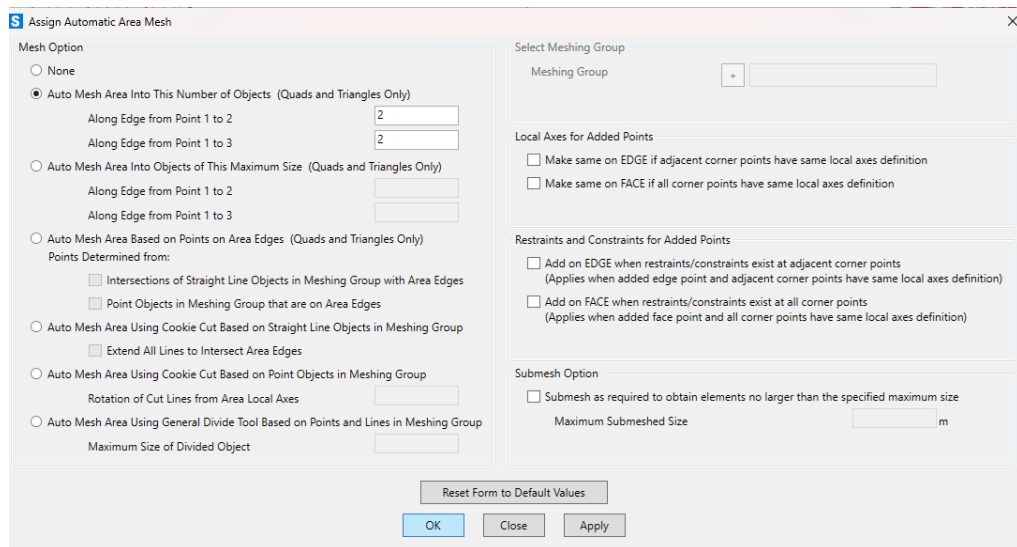




Klik *Select – Properties – Area Sections – Shearwall*. Lalu klik *Assign – Area – Automatic Area Mesh* – pilih “Auto Mesh Area into this Number of Object”.

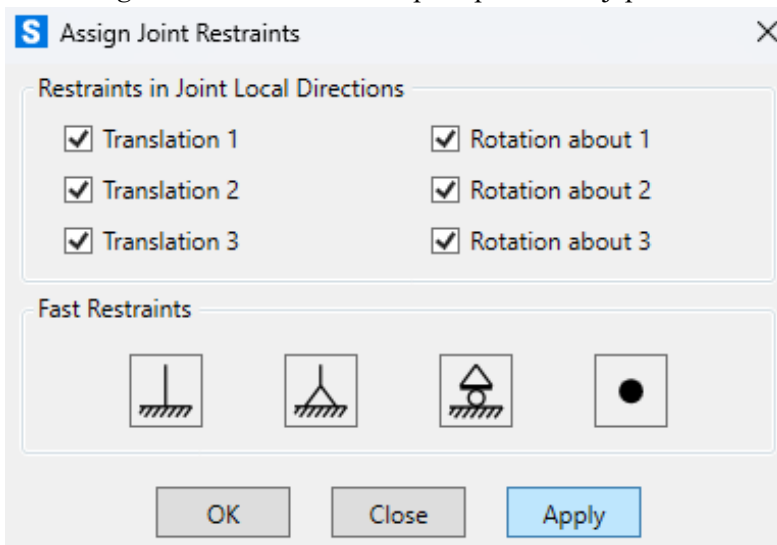






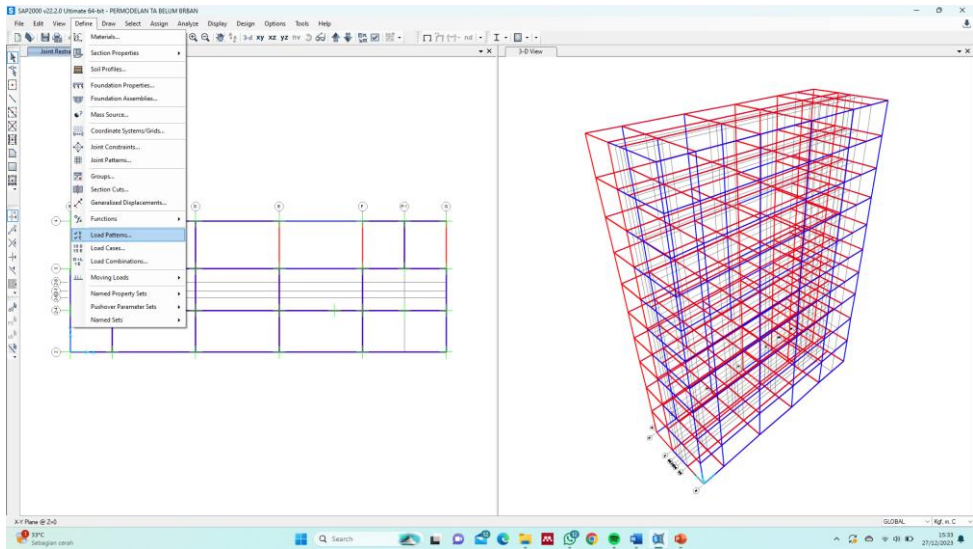
### **Langkah-8: Membuat Perletakan**

Membuat perletakan dapat dilakukan dengan cara pilih dan blok *joint* pada area paling dasar lalu klik *Assign – Joint – Restraints* – pilih perletakan jepit.

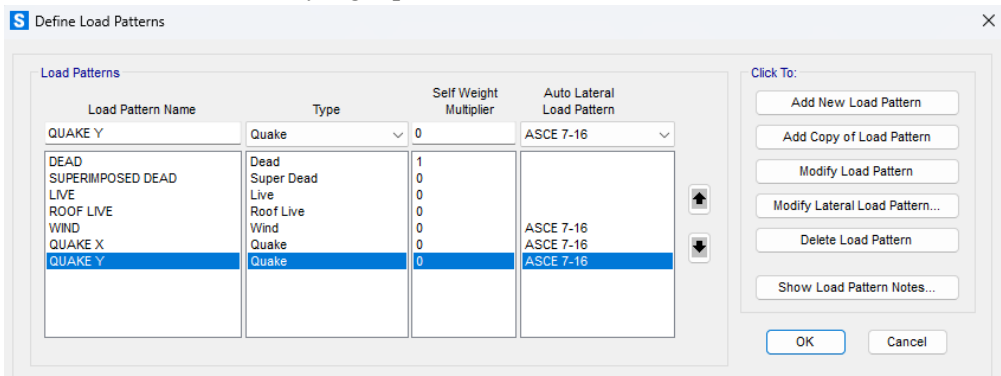


### **Langkah-9: Load Patterns**

Distribusi pembebanan dilakukan dengan cara klik *Define – Load Patterns*.

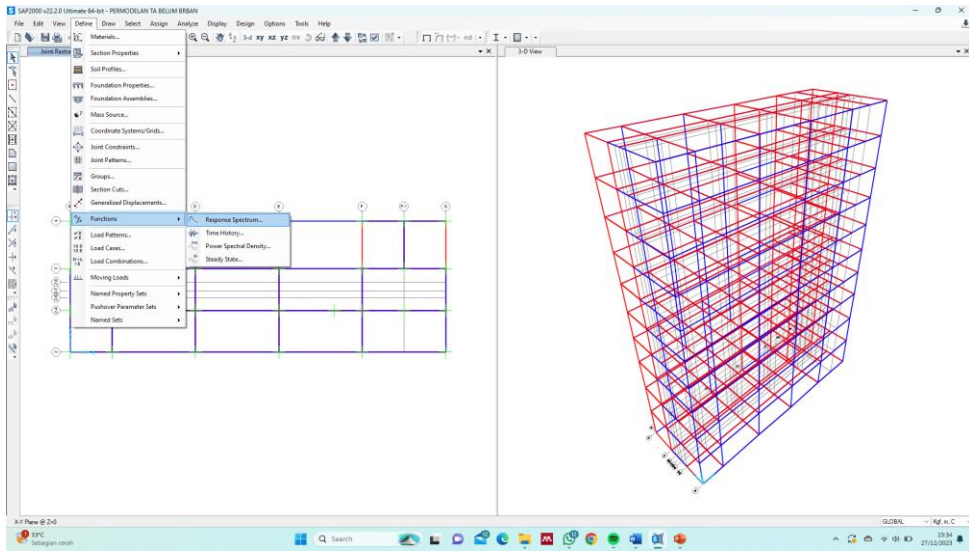


Tambahkan beban-beban yang diperlukan

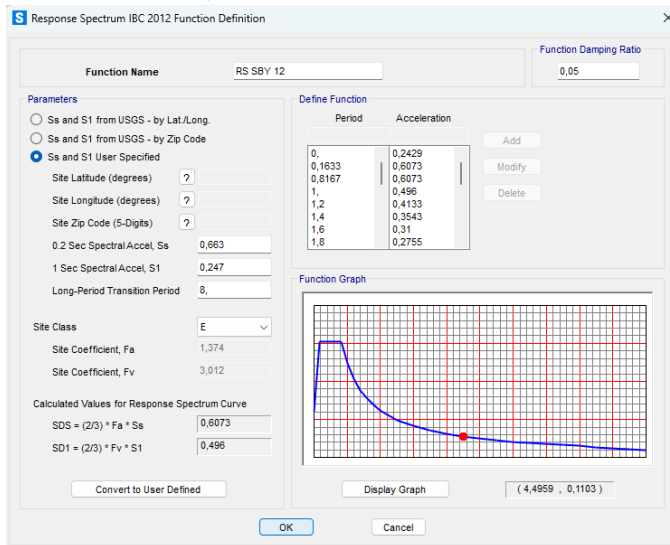


### Langkah-10: Response Spectrum Functions

Memasukkan beban gempa respon spektra dengan cara klik *Define – Functions – Response Spectrum – Add New System*.

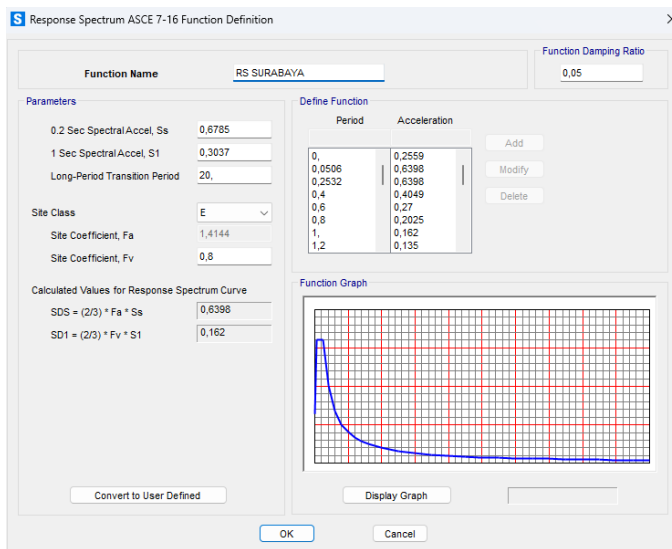


Klik *Add New Function* dan ganti *Type to Add* menjadi IBC 2012, ubah nilai  $S_s$ ,  $S_1$ , dan *Site Class* (SNI 1726:2012)



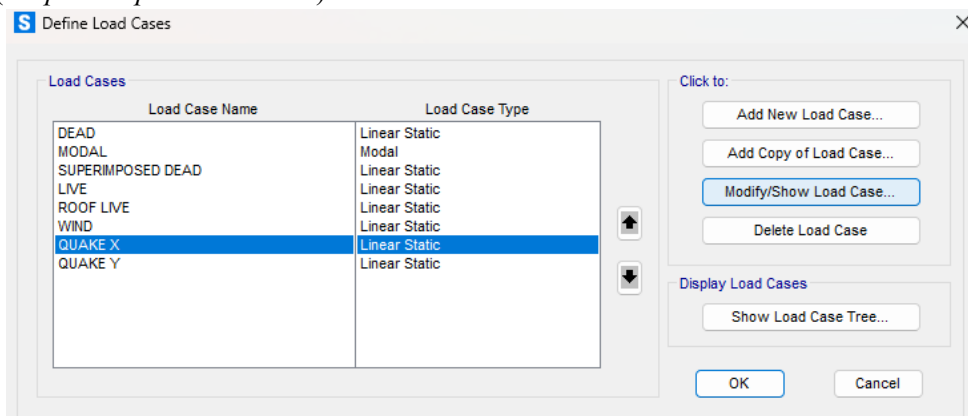
Klik *Add New Function* dan ganti *Type to Add* menjadi ASCE 7-16, ubah nilai  $S_s$ ,  $S_1$ ,  $PGA$ , dan *Site Class* (SNI 1726:2019)





**Langkah-11: Load Cases**

Setelah fungsi gempa dimasukkan, klik *Define – Load Cases – Add New Load Cases* lalu tambahkan beban-beban yang diperlukan. Klik *Modify/Show Load Case* di salah satu beban gempa yang telah ditambahkan sebelumnya. (*Response Spectrum arah X*)



Kemudian ubah *Load Case Type* menjadi *Response Spectrum* kemudian *scale factor* pada *Load Name* diperoleh berdasarkan SNI 1726:2012 dengan faktor  $U_1 = 100\%$  dan  $U_2 = 30\%$ . Dengan perhitungan sebagai berikut:

$$\text{Scale factor } (U_1) = \frac{g \times I_e}{R} = \frac{9,8 \text{ m/s}^2 \times 1,0}{8} = 1,225$$

$$\text{Scale factor } (U_2) = 0,3 \times \frac{g \times I_e}{R} = 0,3 \times \frac{9,8 \text{ m/s}^2 \times 1,0}{8} = 0,3675$$

**S Load Case Data - Response Spectrum**

Load Case Name:  Set Def Name Modify/Show...

Notes

Load Case Type: Response Spectrum Design...

Modal Combination:
 

- CQC
- SRSS
- Absolute
- GMC
- NRC 10 Percent
- Double Sum

 GMC f1: 1, GMC f2: 0, Periodic + Rigid Type: SRSS

Directional Combination:
 

- SRSS
- CQC3
- Absolute

 Scale Factor:

Mass Source: Previous (MSSSRC1)

Diaphragm Eccentricity:
 

- Eccentricity Ratio: 0,
- Override Eccentricities: Override...

Modal Load Case:
 

- Use Modes from this Modal Load Case: MODAL
- Standard - Acceleration Loading
- Advanced - Displacement Inertia Loading

Loads Applied

Load Type	Load Name	Function	Scale Factor
Accel	U1	RS SBY 12	1,225
Accel	U2	RS SBY 12	0,3675

Add Modify Delete

Show Advanced Load Parameters

Other Parameters:
 

- Modal Damping: Constant at 0,05

 Modify/Show...

OK Cancel

(Response Spectrum arah Y)

**S Define Load Cases**

Load Cases

Load Case Name	Load Case Type
DEAD	Linear Static
MODAL	Modal
SUPERIMPOSED DEAD	Linear Static
LIVE	Linear Static
ROOF LIVE	Linear Static
WIND	Linear Static
QUAKE X	Response Spectrum
QUAKE Y	Linear Static

Click to:
 

- Add New Load Case...
- Add Copy of Load Case...
- Modify/Show Load Case...
- Delete Load Case

 Display Load Cases:
 

- Show Load Case Tree...

 OK Cancel

Kemudian ubah *Load Case Type* menjadi *Response Spectrum* kemudian *scale factor* pada *Load Name* diperoleh berdasarkan SNI 1726:2012 dengan faktor  $U1 = 30\%$  dan  $U2 = 100\%$ . Dengan perhitungan sebagai berikut:

$$\text{Scale factor } (U1) = 0,3 \times \frac{g \times I_e}{R} = 0,3 \times \frac{9,8 \text{ m/s}^2 \times 1,0}{8} = 0,3675$$

$$\text{Scale factor } (U2) = \frac{g \times I_e}{R} = \frac{9,8 \text{ m/s}^2 \times 1,0}{8} = 1,225$$

**S Load Case Data - Response Spectrum**

Load Case Name: QUAKE Y    Set Def Name    Modify/Show...

Modal Combination:

- CQC    GMC f1: 1,    GMC f2: 0,
- SRSS    Periodic + Rigid Type: SRSS
- Absolute
- GMC
- NRC 10 Percent
- Double Sum

Modal Load Case:

Use Modes from this Modal Load Case: MODAL

- Standard - Acceleration Loading
- Advanced - Displacement Inertia Loading

Loads Applied:

Load Type	Load Name	Function	Scale Factor
Accel	U1	RS SBY 12	0,3675
Accel	U1	RS SBY 12	0,3675
Accel	U2	RS SBY 12	1,225

Show Advanced Load Parameters

Other Parameters:

Modal Damping: Constant at 0.05    Modify/Show...

Load Case Type: Response Spectrum    Design...

Directional Combination:

- SRSS
- CQC3
- Absolute

Scale Factor: \_\_\_\_\_

Mass Source: Previous (MSSSRC1)

Diaphragm Eccentricity:

Eccentricity Ratio: 0,    Override Eccentricities: Override...

OK    Cancel

**S Define Load Cases**

Load Cases:

Load Case Name	Load Case Type
DEAD	Linear Static
MODAL	Modal
SUPERIMPOSED DEAD	Linear Static
LIVE	Linear Static
ROOF LIVE	Linear Static
WIND	Linear Static
QUAKE X	Response Spectrum
QUAKE Y	Response Spectrum

Click to:

Add New Load Case...  
Add Copy of Load Case...  
Modify/Show Load Case...  
Delete Load Case

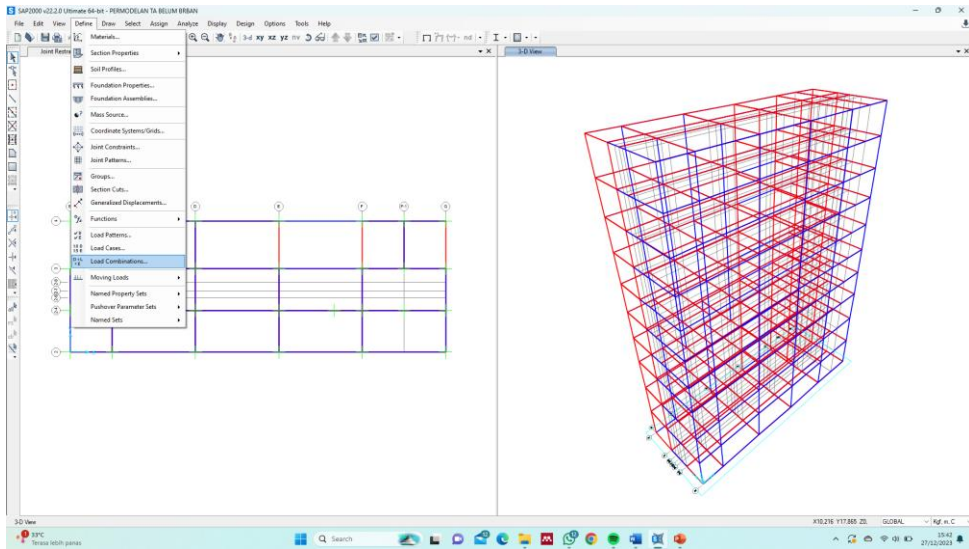
Display Load Cases:

Show Load Case Tree...

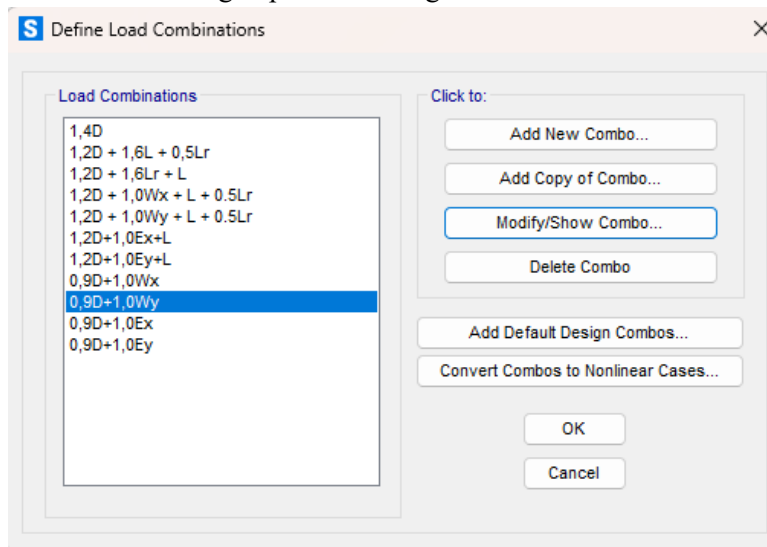
OK    Cancel

### **Langkah-12: Load Combinations**

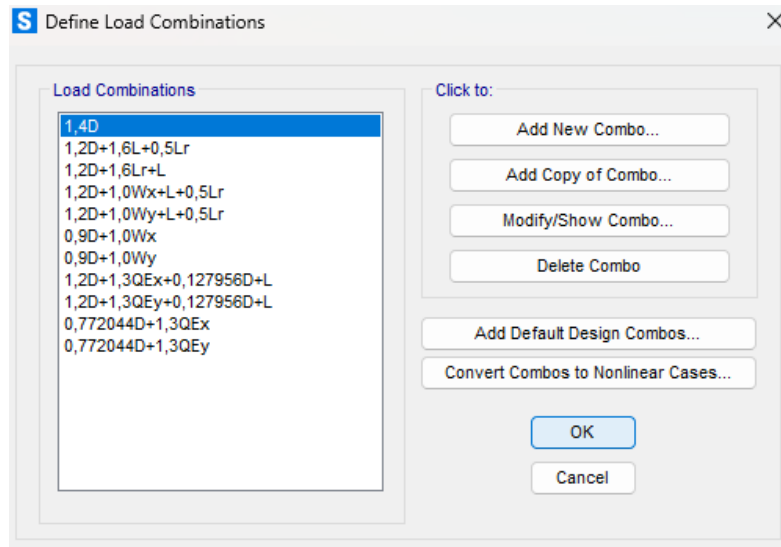
Selanjutnya memasukkan beban gempa dari *Load Combinations* dengan cara klik *Define – Load Combinations – Add New Combo*.



Kemudian membuat beban gempa sesuai dengan SNI 1726:2012.

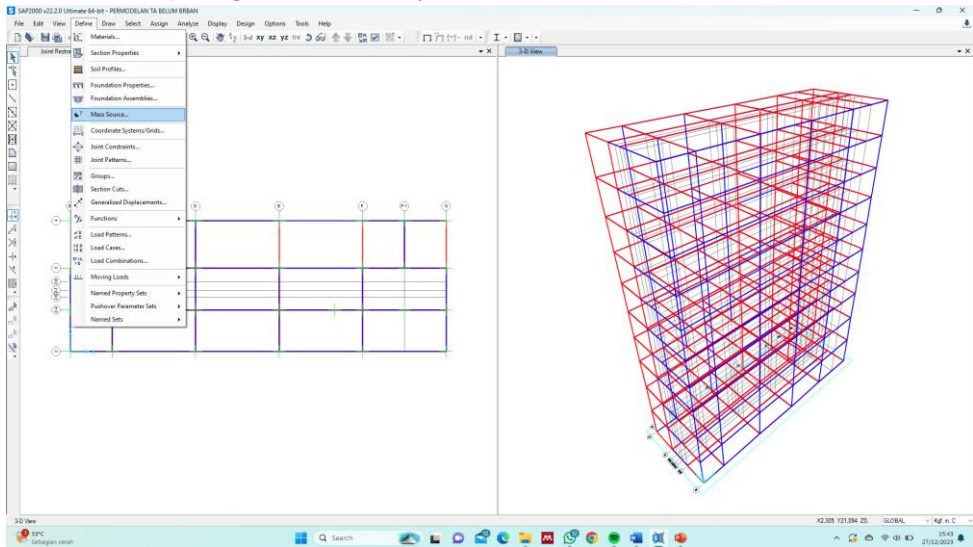


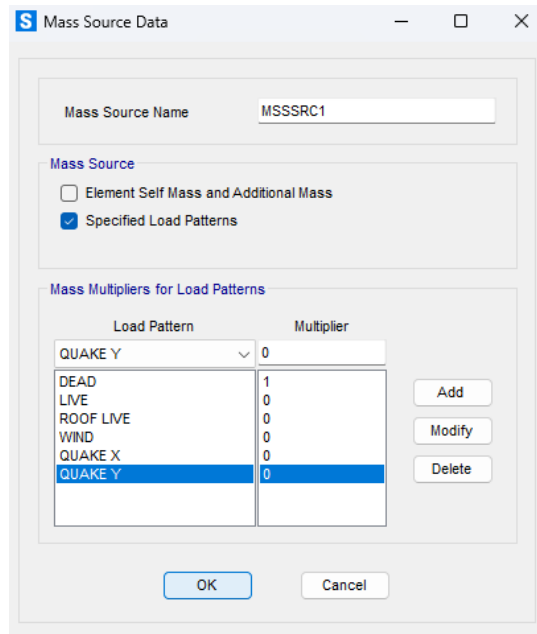
Kemudian membuat beban gempa sesuai dengan SNI 1726:2019.



### **Langkah-13: Mass Source**

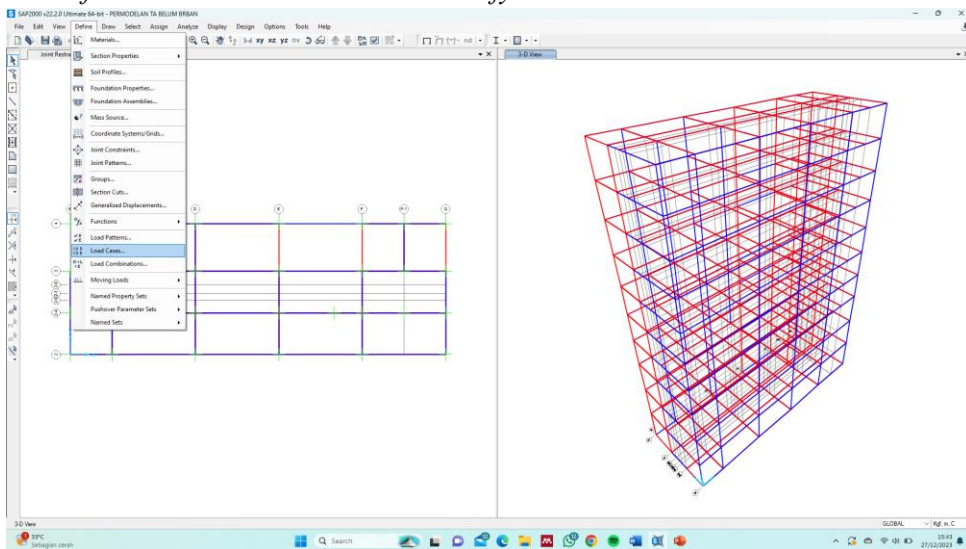
Setelah beban diinput langkah selanjutnya yaitu menentukan *Mass Source* (Faktor Reduksi Beban) dengan cara klik *Define – Mass Source – Add New Mass Source*.

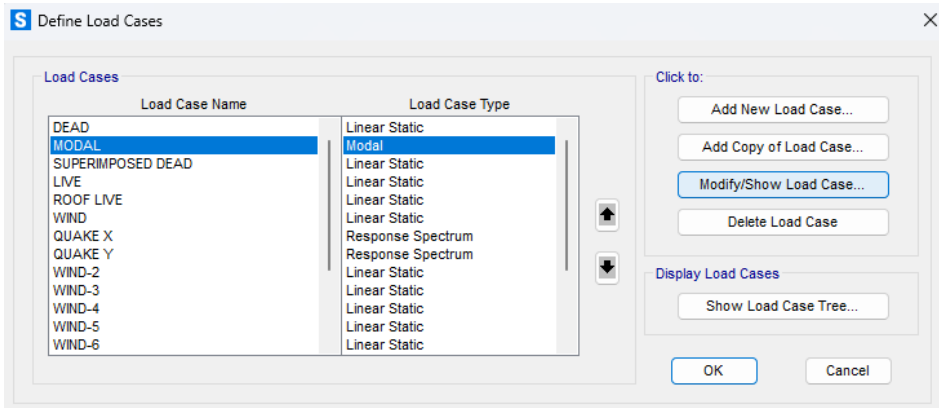




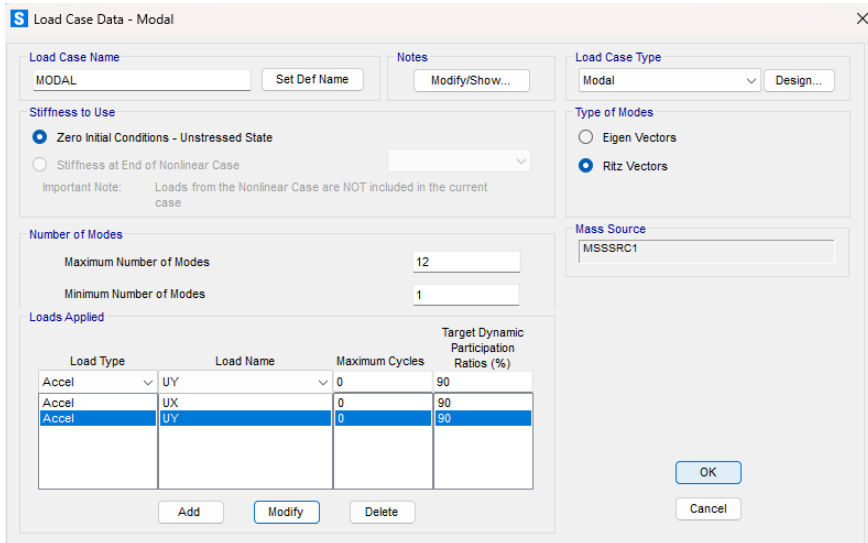
### **Langkah-14: Modal**

Klik *Define – Load Cases – Modal – Modify/Show Load Case.*

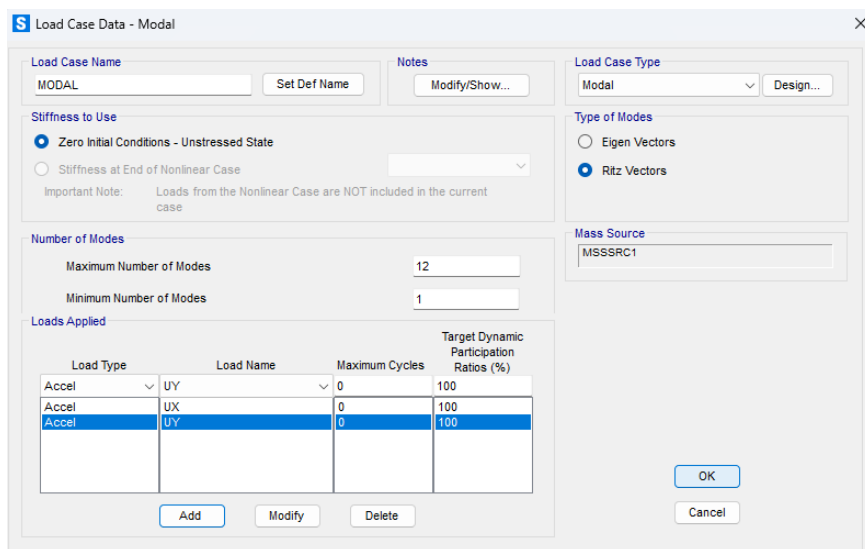




Ubah *Type of Modes* menjadi “*Ritz Vectors*” dan isi *Target Dynamic Participation Ratios (%)* menjadi 90 (berdasarkan SNI 1726:2012 Pasal 7.9.1).



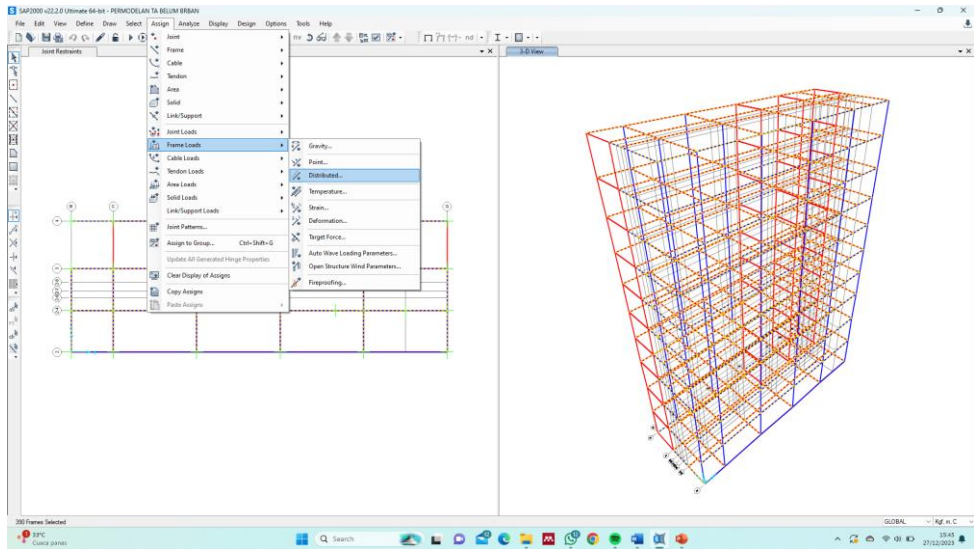
Ubah *Type of Modes* menjadi “*Ritz Vectors*” dan isi *Target Dynamic Participation Ratios (%)* menjadi 100 (berdasarkan SNI 1726:2019 Pasal 7.9.1.1).



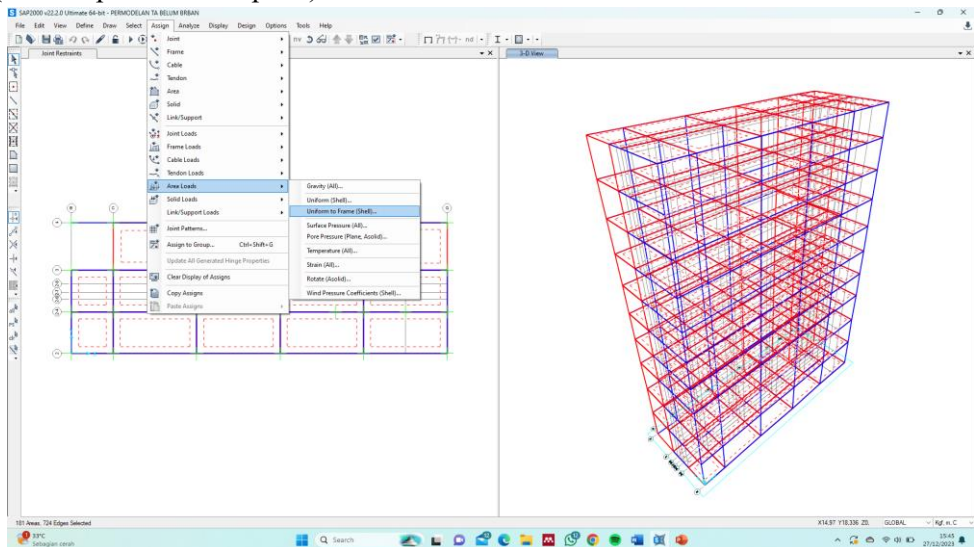
### **Langkah-15: Distribusi Beban Mati dan Beban Hidup**

Langkah selanjutnya yaitu memasukkan beban hidup dan beban mati yang telah dihitung sebelumnya, kemudian masukkan ke dalam pembebanan balok dan pelat. Untuk pembebanan balok dilakukan dengan cara klik *Select – Properties – Frame Sections*. Lalu pilih balok yang ditinjau kemudian klik *Assign – Frame Loads – Distributed*. Isi kolom *Uniform Load* dengan beban yang sudah dihitung sebelumnya. Untuk pembebanan pelat dilakukan dengan cara klik *Select – Properties – Area Sections*. Lalu pilih pelat yang ditinjau kemudian klik *Assign – Area Loads – Uniform Area (Shell)*. Lalu isi dikolom *Load* beban pelat yang sudah dihitung sebelumnya. (Contoh pembebanan balok)



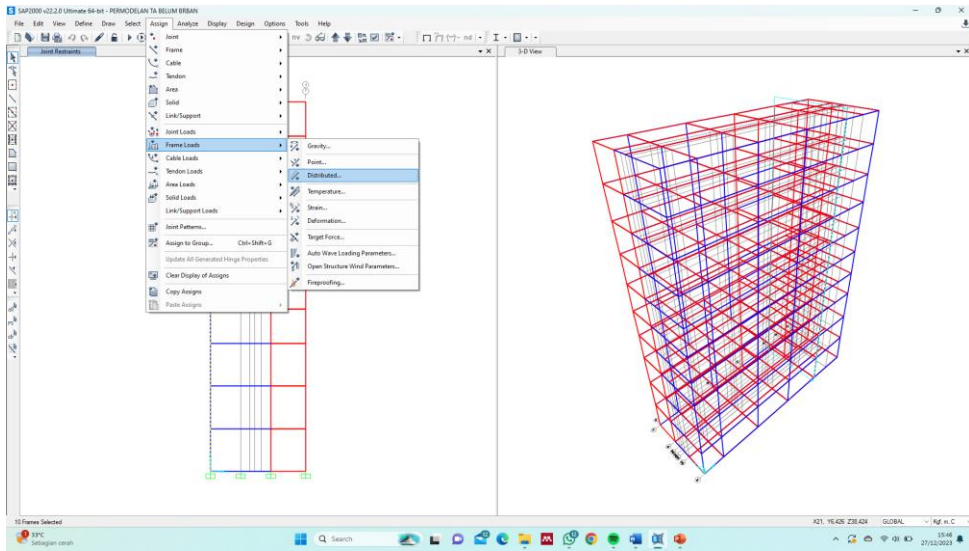


(Contoh pembebanan pelat)



### **Langkah-16: Distribusi Beban Angin**

Beban angin didistribusikan pada tiap as sesuai dengan Tabel 4.18, Tabel 4.19, dan Tabel 4.20. Kemudian pilih as yang akan didistribusikan beban angin tersebut, klik *Assign – Frame Loads – Distributed*.



**S Assign Frame Distributed Loads**

**General**

Load Pattern: WIND

Coordinate System: GLOBAL

Load Direction: Gravity

Load Type: Force

**Options**

Add to Existing Loads

Replace Existing Loads

Delete Existing Loads

Uniform Load: 235,56 kgf/m

**Trapezoidal Loads**

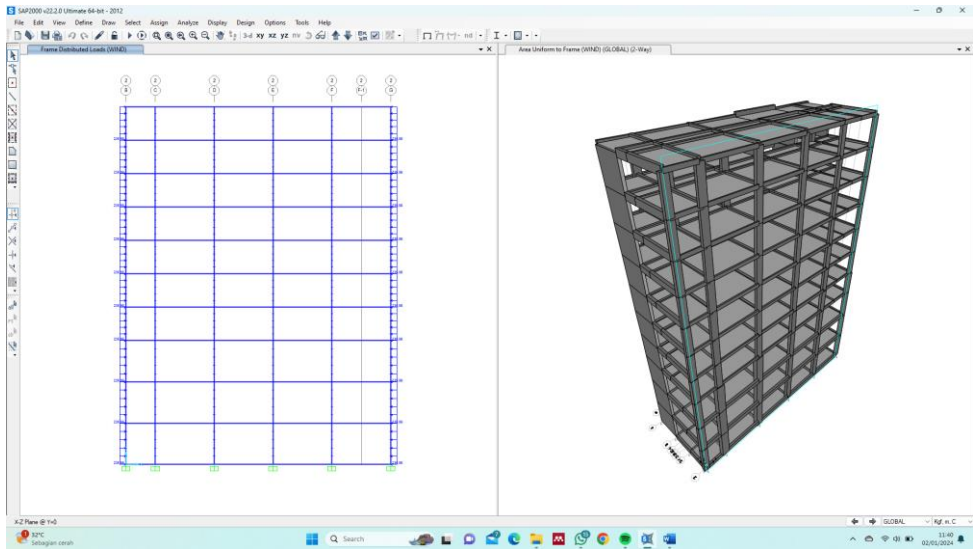
	1.	2.	3.	4.
Relative Distance	0	0,25	0,75	1
Loads	0	0	0	0

kgf/m

Relative Distance from End-I  Absolute Distance from End-I

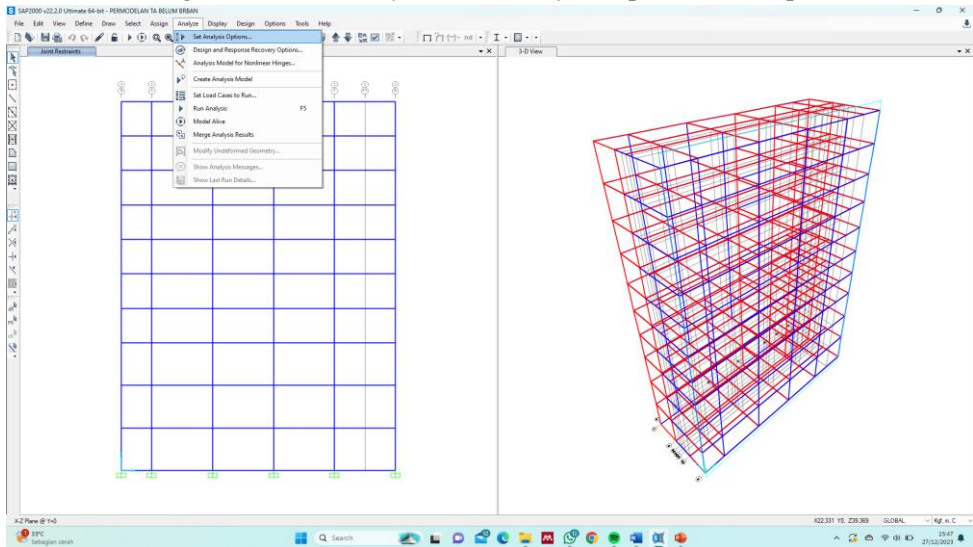
Reset Form to Default Values

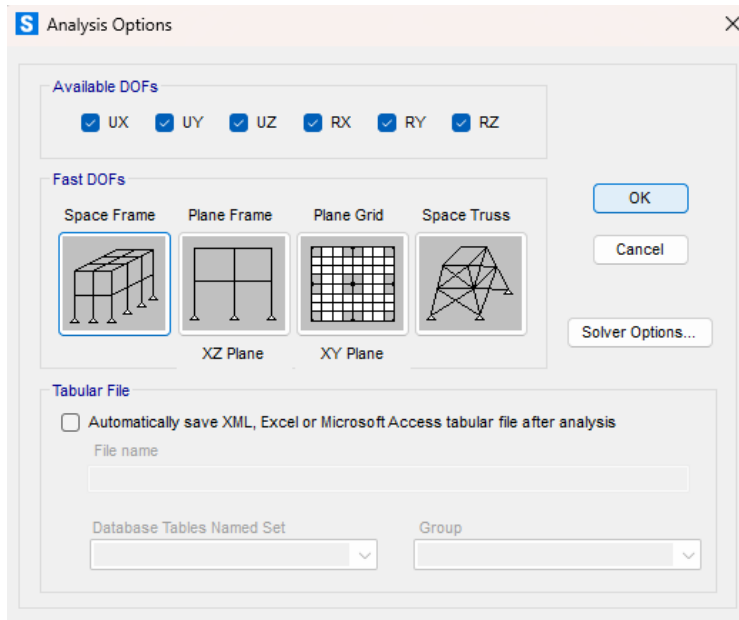
OK Close Apply



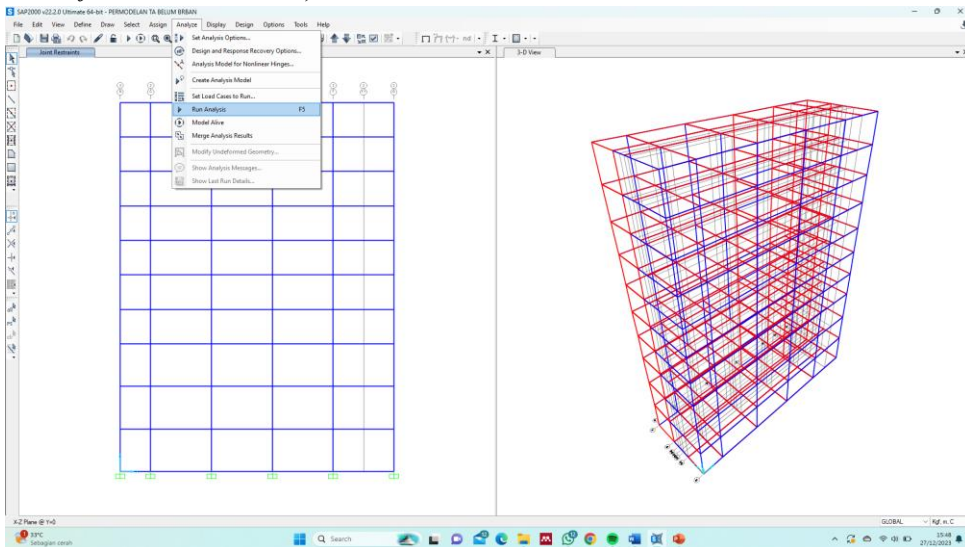
### **Langkah-17: Running Analysis Permodelan**

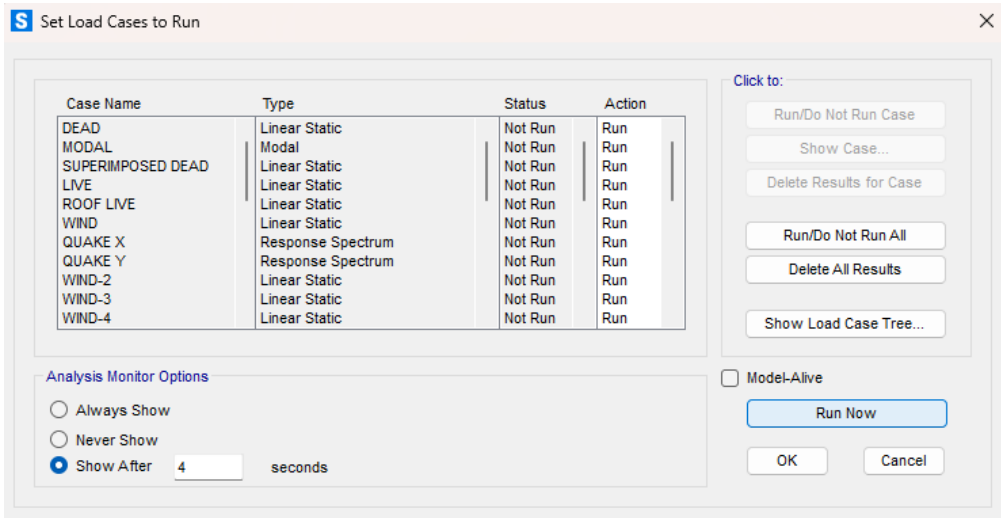
Setelah semua langkah selesai dimasukkan, tahap selanjutnya yaitu *running analysis* permodelan dengan cara klik *Analyze – Set Analysis Option – klik Space Frame*.





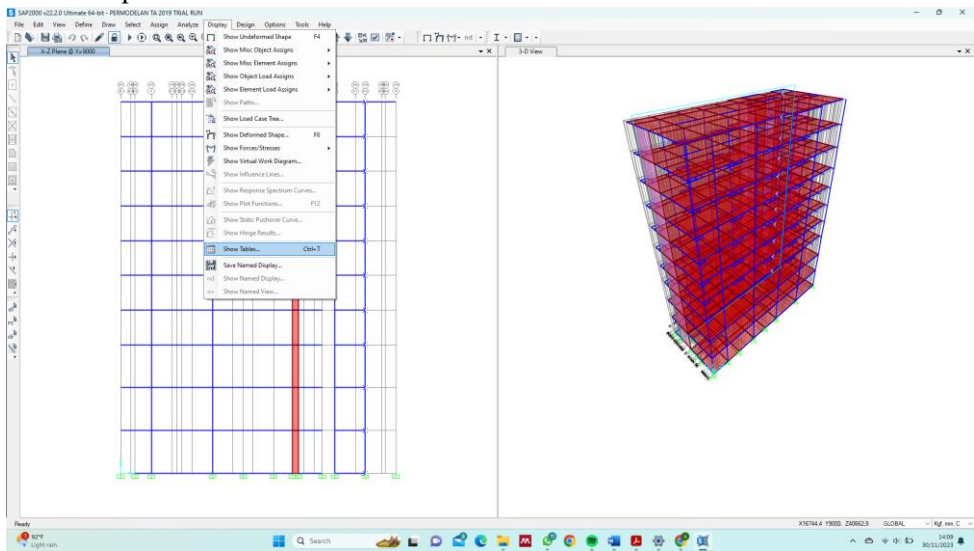
*Run Analysis – Run Now* (untuk menghindari kesalahan saat proses *running* sebaiknya *save as file* terlebih dahulu).

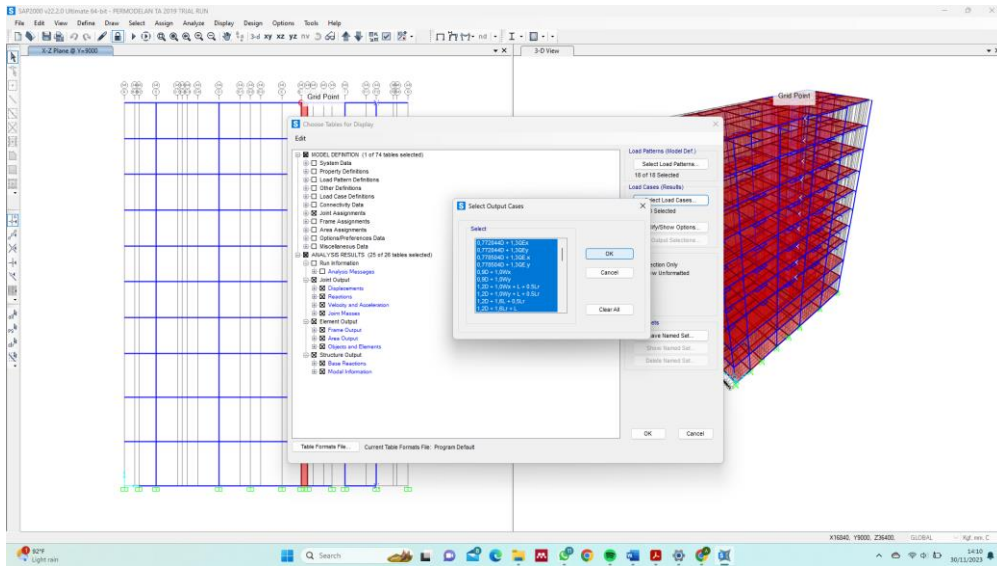




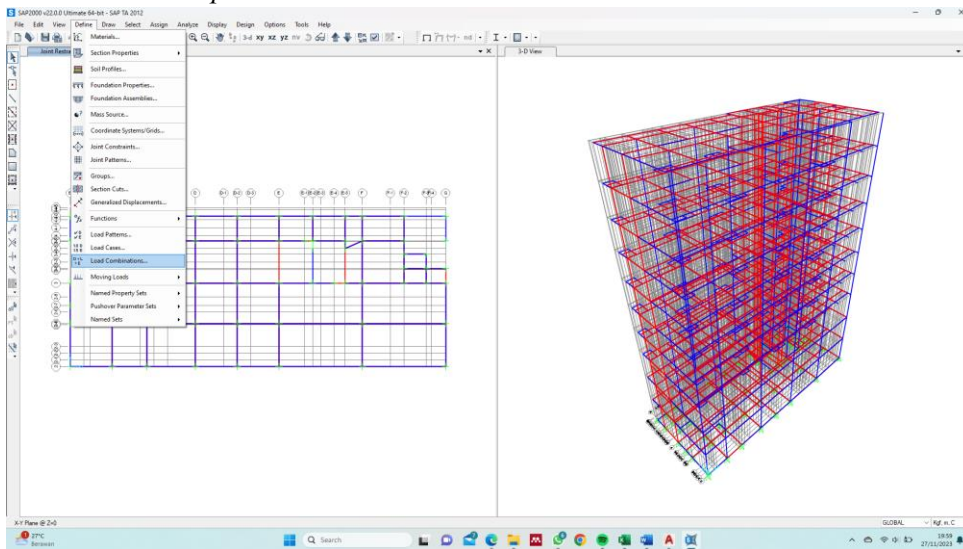
**Langkah-18: Export Table**

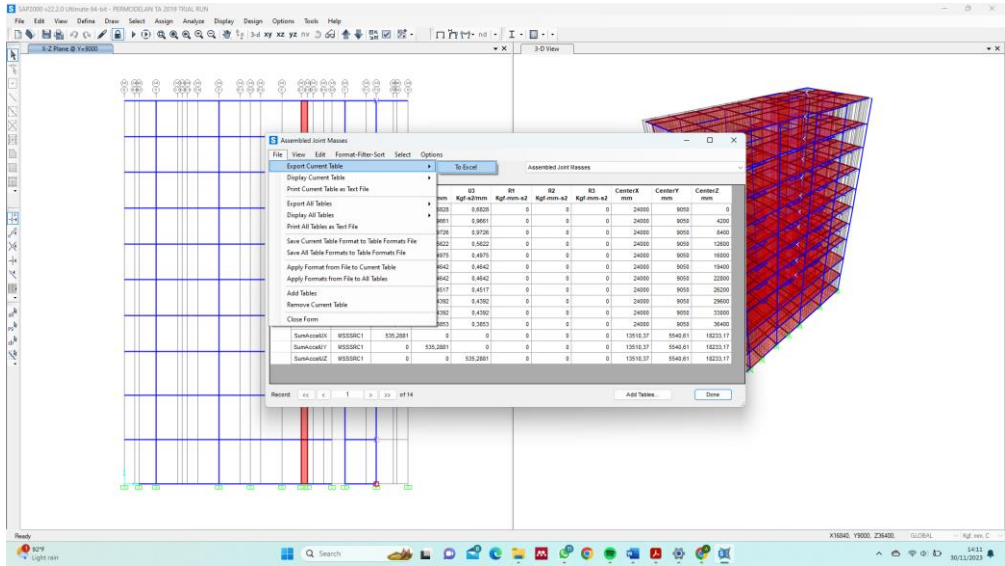
Langkah terakhir yaitu setelah proses Run klik *Display – Show Tables (Ctrl+T) – Analysis Result – Element Output – Frame Output – Select Load Cases* – pilih semua kombinasi pembebanan.





Lalu klik *File – Export All Tables to Excel.*





## LAMPIRAN II

### PERHITUNGAN SIMPANGAN

#### SNI 1726:2012 (Arah X)

$$\begin{aligned}\delta_{1e} &= \delta_{1e} - \delta_{0e} \\ &= 3,122488 \text{ mm} - 0 \\ &= 3,122488 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{2e} &= \delta_{2e} - \delta_{1e} \\ &= 9,211323 \text{ mm} - 3,122488 \text{ mm} \\ &= 6,088835 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{3e} &= \delta_{3e} - \delta_{2e} \\ &= 16,754321 \text{ mm} - 9,211323 \text{ mm} \\ &= 7,542998 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{4e} &= \delta_{4e} - \delta_{3e} \\ &= 22,878135 \text{ mm} - 16,754321 \text{ mm} \\ &= 6,123814 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{5e} &= \delta_{5e} - \delta_{4e} \\ &= 29,102049 \text{ mm} - 22,878135 \text{ mm} \\ &= 6,223914 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{6e} &= \delta_{6e} - \delta_{5e} \\ &= 35,075179 \text{ mm} - 29,102049 \text{ mm} \\ &= 5,97313 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{7e} &= \delta_{7e} - \delta_{6e} \\ &= 40,577087 \text{ mm} - 35,075179 \text{ mm} \\ &= 5,501908 \text{ mm}\end{aligned}$$

#### SNI 1726:2019 (Arah X)

$$\begin{aligned}\delta_{1e} &= \delta_{1e} - \delta_{0e} \\ &= 3,744073 \text{ mm} - 0 \\ &= 3,744073 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{2e} &= \delta_{2e} - \delta_{1e} \\ &= 11,06743 \text{ mm} - 3,744073 \text{ mm} \\ &= 7,323357 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{3e} &= \delta_{3e} - \delta_{2e} \\ &= 20,13704 \text{ mm} - 11,06743 \text{ mm} \\ &= 9,069606 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{4e} &= \delta_{4e} - \delta_{3e} \\ &= 27,49513 \text{ mm} - 20,13704 \text{ mm} \\ &= 7,358092 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{5e} &= \delta_{5e} - \delta_{4e} \\ &= 34,95397 \text{ mm} - 27,495128 \text{ mm} \\ &= 7,458837 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{6e} &= \delta_{6e} - \delta_{5e} \\ &= 42,074286 \text{ mm} - 34,953965 \text{ mm} \\ &= 7,120321 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{7e} &= \delta_{7e} - \delta_{6e} \\ &= 48,576497 \text{ mm} - 42,074286 \text{ mm} \\ &= 6,502211 \text{ mm}\end{aligned}$$



$$\begin{aligned}\delta_{8e} &= \delta_{8e} - \delta_{7e} \\ &= 45,606565 \text{ mm} - 40,577087 \text{ mm} \\ &= 5,029478 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{8e} &= \delta_{8e} - \delta_{7e} \\ &= 54,445151 \text{ mm} - 48,576497 \text{ mm} \\ &= 5,868654 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{9e} &= \delta_{9e} - \delta_{8e} \\ &= 49,952583 \text{ mm} - 45,606565 \text{ mm} \\ &= 4,346018 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{9e} &= \delta_{9e} - \delta_{8e} \\ &= 59,423962 \text{ mm} - 54,445151 \text{ mm} \\ &= 4,978811 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{10e} &= \delta_{10e} - \delta_{9e} \\ &= 53,430259 \text{ mm} - 49,952583 \text{ mm} \\ &= 3,477676 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{10e} &= \delta_{10e} - \delta_{9e} \\ &= 63,30101 \text{ mm} - 59,423962 \text{ mm} \\ &= 3,877048 \text{ mm}\end{aligned}$$

**SNI 1726:2012 (Arah X)**

$$\begin{aligned}\delta_1 &= \frac{C_d \times \delta_{1e}}{I_e} \\ &= \frac{5,5 \times 3,122488 \text{ mm}}{1,00} \\ &= 17,174 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_1 &= \frac{C_d \times \delta_{1e}}{I_e} \\ &= \frac{5,5 \times 3,744073 \text{ mm}}{1,00} \\ &= 20,5924 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_2 &= \frac{C_d \times \delta_{2e}}{I_e} \\ &= \frac{5,5 \times 6,088835 \text{ mm}}{1} \\ &= 33,489 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_2 &= \frac{C_d \times \delta_{2e}}{I_e} \\ &= \frac{5,5 \times 7,323357 \text{ mm}}{1} \\ &= 40,2785 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_3 &= \frac{C_d \times \delta_{3e}}{I_e} \\ &= \frac{5,5 \times 7,542998 \text{ mm}}{1} \\ &= 41,486 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_3 &= \frac{C_d \times \delta_{3e}}{I_e} \\ &= \frac{5,5 \times 9,069606 \text{ mm}}{1} \\ &= 49,8828 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_4 &= \frac{C_d \times \delta_{4e}}{I_e} \\ &= \frac{5,5 \times 6,123814 \text{ mm}}{1} \\ &= 33,681 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_5 &= \frac{C_d \times \delta_{5e}}{I_e} \\ &= \frac{5,5 \times 6,223914 \text{ mm}}{1} \\ &= 34,232 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_6 &= \frac{C_d \times \delta_{6e}}{I_e} \\ &= \frac{5,5 \times 5,97313 \text{ mm}}{1} \\ &= 32,852 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_7 &= \frac{C_d \times \delta_{7e}}{I_e} \\ &= \frac{5,5 \times 5,501908 \text{ mm}}{1} \\ &= 30,260 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_8 &= \frac{C_d \times \delta_{8e}}{I_e} \\ &= \frac{5,5 \times 5,029478 \text{ mm}}{1} \\ &= 27,662 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_9 &= \frac{C_d \times \delta_{9e}}{I_e} \\ &= \frac{5,5 \times 4,346018 \text{ mm}}{1} \\ &= 23,903 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_4 &= \frac{C_d \times \delta_{4e}}{I_e} \\ &= \frac{5,5 \times 7,358092 \text{ mm}}{1} \\ &= 40,4695 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_5 &= \frac{C_d \times \delta_{5e}}{I_e} \\ &= \frac{5,5 \times 7,458837 \text{ mm}}{1} \\ &= 41,0236 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_6 &= \frac{C_d \times \delta_{6e}}{I_e} \\ &= \frac{5,5 \times 7,120321 \text{ mm}}{1} \\ &= 39,1618 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_7 &= \frac{C_d \times \delta_{7e}}{I_e} \\ &= \frac{5,5 \times 6,502211 \text{ mm}}{1} \\ &= 35,7622 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_8 &= \frac{C_d \times \delta_{8e}}{I_e} \\ &= \frac{5,5 \times 5,868654 \text{ mm}}{1} \\ &= 32,2776 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_9 &= \frac{C_d \times \delta_{9e}}{I_e} \\ &= \frac{5,5 \times 4,978811 \text{ mm}}{1} \\ &= 27,3835 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{10} &= \frac{C_d \times \delta_{10e}}{I_e} \\ &= \frac{5,5 \times 3,477676 \text{ mm}}{1} \\ &= 19,127 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{10} &= \frac{C_d \times \delta_{10e}}{I_e} \\ &= \frac{5,5 \times 3,877048 \text{ mm}}{1} \\ &= 21,3238 \text{ mm}\end{aligned}$$

**SNI 1726:2012 (Arah X)**

$$\begin{aligned}\Delta_1 &\leq \Delta_{ijin} \\ 17,174 \text{ mm} &\leq 64,615 \text{ mm} \\ &\text{(Memenuhi Persyaratan)}\end{aligned}$$

$$\begin{aligned}\Delta_2 &\leq \Delta_{ijin} \\ 33,489 \text{ mm} &\leq 64,615 \text{ mm} \\ &\text{(Memenuhi Persyaratan)}\end{aligned}$$

$$\begin{aligned}\Delta_3 &\leq \Delta_{ijin} \\ 41,486 \text{ mm} &\leq 64,615 \text{ mm} \\ &\text{(Memenuhi Persyaratan)}\end{aligned}$$

$$\begin{aligned}\Delta_4 &\leq \Delta_{ijin} \\ 33,681 \text{ mm} &\leq 52,308 \text{ mm} \\ &\text{(Memenuhi Persyaratan)}\end{aligned}$$

$$\begin{aligned}\Delta_5 &\leq \Delta_{ijin} \\ 34,232 \text{ mm} &\leq 52,308 \text{ mm} \\ &\text{(Memenuhi Persyaratan)}\end{aligned}$$

$$\begin{aligned}\Delta_6 &\leq \Delta_{ijin} \\ 32,852 \text{ mm} &\leq 52,308 \text{ mm} \\ &\text{(Memenuhi Persyaratan)}\end{aligned}$$

**SNI 1726:2019 (Arah X)**

$$\begin{aligned}\Delta_1 &\leq \Delta_{ijin} \\ 20,592 \text{ mm} &\leq 64,615 \text{ mm} \\ &\text{(Memenuhi Persyaratan)}\end{aligned}$$

$$\begin{aligned}\Delta_2 &\leq \Delta_{ijin} \\ 40,278 \text{ mm} &\leq 64,615 \text{ mm} \\ &\text{(Memenuhi Persyaratan)}\end{aligned}$$

$$\begin{aligned}\Delta_3 &\leq \Delta_{ijin} \\ 49,883 \text{ mm} &\leq 64,615 \text{ mm} \\ &\text{(Memenuhi Persyaratan)}\end{aligned}$$

$$\begin{aligned}\Delta_4 &\leq \Delta_{ijin} \\ 40,470 \text{ mm} &\leq 52,308 \text{ mm} \\ &\text{(Memenuhi Persyaratan)}\end{aligned}$$

$$\begin{aligned}\Delta_5 &\leq \Delta_{ijin} \\ 41,024 \text{ mm} &\leq 52,308 \text{ mm} \\ &\text{(Memenuhi Persyaratan)}\end{aligned}$$

$$\begin{aligned}\Delta_6 &\leq \Delta_{ijin} \\ 39,162 \text{ mm} &\leq 52,308 \text{ mm} \\ &\text{(Memenuhi Persyaratan)}\end{aligned}$$

$$\begin{aligned} \Delta_7 &\leq \Delta_{ijin} \\ 30,260 \text{ mm} &\leq 52,308 \text{ mm} \\ &\text{(Memenuhi Persyaratan)} \end{aligned}$$

$$\begin{aligned} \Delta_8 &\leq \Delta_{ijin} \\ 27,662 \text{ mm} &\leq 52,308 \text{ mm} \\ &\text{(Memenuhi Persyaratan)} \end{aligned}$$

$$\begin{aligned} \Delta_9 &\leq \Delta_{ijin} \\ 23,903 \text{ mm} &\leq 52,308 \text{ mm} \\ &\text{(Memenuhi Persyaratan)} \end{aligned}$$

$$\begin{aligned} \Delta_{10} &\leq \Delta_{ijin} \\ 19,127 \text{ mm} &\leq 52,308 \text{ mm} \\ &\text{(Memenuhi Persyaratan)} \end{aligned}$$

$$\begin{aligned} \Delta_7 &\leq \Delta_{ijin} \\ 35,762 \text{ mm} &\leq 52,308 \text{ mm} \\ &\text{(Memenuhi Persyaratan)} \end{aligned}$$

$$\begin{aligned} \Delta_8 &\leq \Delta_{ijin} \\ 32,278 \text{ mm} &\leq 52,308 \text{ mm} \\ &\text{(Memenuhi Persyaratan)} \end{aligned}$$

$$\begin{aligned} \Delta_9 &\leq \Delta_{ijin} \\ 27,383 \text{ mm} &\leq 52,308 \text{ mm} \\ &\text{(Memenuhi Persyaratan)} \end{aligned}$$

$$\begin{aligned} \Delta_{10} &\leq \Delta_{ijin} \\ 21,324 \text{ mm} &\leq 52,308 \text{ mm} \\ &\text{(Memenuhi Persyaratan)} \end{aligned}$$

#### SNI 1726:2012 (Arah Y)

$$\begin{aligned} \delta_{1e} &= \delta_{1e} - \delta_{0e} \\ &= 1,540086 \text{ mm} - 0 \\ &= 1,540086 \text{ mm} \end{aligned}$$

$$\begin{aligned} \delta_{2e} &= \delta_{2e} - \delta_{1e} \\ &= 5,395003 \text{ mm} - 1,540086 \text{ mm} \\ &= 3,854917 \text{ mm} \end{aligned}$$

$$\begin{aligned} \delta_{3e} &= \delta_{3e} - \delta_{2e} \\ &= 10,855469 \text{ mm} - 5,395003 \text{ mm} \\ &= 5,460466 \text{ mm} \end{aligned}$$

$$\begin{aligned} \delta_{4e} &= \delta_{4e} - \delta_{3e} \\ &= 16,056182 \text{ mm} - 10,855469 \text{ mm} \\ &= 5,200713 \text{ mm} \end{aligned}$$

#### SNI 1726:2019 (Arah Y)

$$\begin{aligned} \delta_{1e} &= \delta_{1e} - \delta_{0e} \\ &= 1,849059 \text{ mm} - 0 \\ &= 1,849059 \text{ mm} \end{aligned}$$

$$\begin{aligned} \delta_{2e} &= \delta_{2e} - \delta_{1e} \\ &= 6,421049 \text{ mm} - 1,849059 \text{ mm} \\ &= 4,57199 \text{ mm} \end{aligned}$$

$$\begin{aligned} \delta_{3e} &= \delta_{3e} - \delta_{2e} \\ &= 20,137036 \text{ mm} - 11,06743 \text{ mm} \\ &= 9,069606 \text{ mm} \end{aligned}$$

$$\begin{aligned} \delta_{4e} &= \delta_{4e} - \delta_{3e} \\ &= 19,037296 \text{ mm} - 12,905046 \text{ mm} \\ &= 6,13225 \text{ mm} \end{aligned}$$

$$\begin{aligned}\delta_{5e} &= \delta_{5e} - \delta_{4e} \\ &= 21,733125 \text{ mm} - 16,056182 \text{ mm} \\ &= 5,676943 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{5e} &= \delta_{5e} - \delta_{4e} \\ &= 25,748034 \text{ mm} - 19,037296 \text{ mm} \\ &= 6,710738 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{6e} &= \delta_{6e} - \delta_{5e} \\ &= 27,715595 \text{ mm} - 21,733125 \text{ mm} \\ &= 5,98247 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{6e} &= \delta_{6e} - \delta_{5e} \\ &= 32,790471 \text{ mm} - 25,748034 \text{ mm} \\ &= 7,042437 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{7e} &= \delta_{7e} - \delta_{6e} \\ &= 33,851268 \text{ mm} - 27,715595 \text{ mm} \\ &= 6,135673 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{7e} &= \delta_{7e} - \delta_{6e} \\ &= 39,981901 \text{ mm} - 32,790471 \text{ mm} \\ &= 7,19143 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{8e} &= \delta_{8e} - \delta_{7e} \\ &= 40,013505 \text{ mm} - 33,851268 \text{ mm} \\ &= 6,162237 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{8e} &= \delta_{8e} - \delta_{7e} \\ &= 47,190193 \text{ mm} - 39,981901 \text{ mm} \\ &= 7,208292 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{9e} &= \delta_{9e} - \delta_{8e} \\ &= 46,115335 \text{ mm} - 40,013505 \text{ mm} \\ &= 6,10183 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{9e} &= \delta_{9e} - \delta_{8e} \\ &= 54,24308 \text{ mm} - 47,190193 \text{ mm} \\ &= 7,052887 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{10e} &= \delta_{10e} - \delta_{9e} \\ &= 52,157517 \text{ mm} - 46,115335 \text{ mm} \\ &= 6,042182 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{10e} &= \delta_{10e} - \delta_{9e} \\ &= 61,239029 \text{ mm} - 54,24308 \text{ mm} \\ &= 1,749917 \text{ mm}\end{aligned}$$

#### SNI 1726:2012 (Arah Y)

$$\begin{aligned}\delta_1 &= \frac{C_d \times \delta_{1e}}{I_e} \\ &= \frac{5,5 \times 1,540086 \text{ mm}}{1,00} \\ &= 8,470 \text{ mm}\end{aligned}$$

#### SNI 1726:2019 (Arah Y)

$$\begin{aligned}\delta_1 &= \frac{C_d \times \delta_{1e}}{I_e} \\ &= \frac{5,5 \times 1,849059 \text{ mm}}{1,00} \\ &= 10,1698 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_2 &= \frac{C_d \times \delta_{2e}}{I_e} \\ &= \frac{5,5 \times 3,854917 \text{ mm}}{1} \\ &= 21,202 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_2 &= \frac{C_d \times \delta_{2e}}{I_e} \\ &= \frac{5,5 \times 4,57199 \text{ mm}}{1} \\ &= 25,1459 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_3 &= \frac{C_d \times \delta_{3e}}{I_e} \\ &= \frac{5,5 \times 5,460466 \text{ mm}}{1} \\ &= 30,033 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_3 &= \frac{C_d \times \delta_{3e}}{I_e} \\ &= \frac{5,5 \times 6,483997 \text{ mm}}{1} \\ &= 35,6620 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_4 &= \frac{C_d \times \delta_{4e}}{I_e} \\ &= \frac{5,5 \times 5,200713 \text{ mm}}{1} \\ &= 28,604 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_4 &= \frac{C_d \times \delta_{4e}}{I_e} \\ &= \frac{5,5 \times 6,13225 \text{ mm}}{1} \\ &= 33,7274 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_5 &= \frac{C_d \times \delta_{5e}}{I_e} \\ &= \frac{5,5 \times 5,676943 \text{ mm}}{1} \\ &= 31,223 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_5 &= \frac{C_d \times \delta_{5e}}{I_e} \\ &= \frac{5,5 \times 6,710738 \text{ mm}}{1} \\ &= 36,9091 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_6 &= \frac{C_d \times \delta_{6e}}{I_e} \\ &= \frac{5,5 \times 5,98247 \text{ mm}}{1} \\ &= 32,904 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_6 &= \frac{C_d \times \delta_{6e}}{I_e} \\ &= \frac{5,5 \times 7,042437 \text{ mm}}{1} \\ &= 38,7334 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_7 &= \frac{C_d \times \delta_{7e}}{I_e} \\ &= \frac{5,5 \times 6,135673 \text{ mm}}{1} \\ &= 33,746 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_7 &= \frac{C_d \times \delta_{7e}}{I_e} \\ &= \frac{5,5 \times 7,19143 \text{ mm}}{1} \\ &= 39,5529 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_8 &= \frac{C_d \times \delta_{8e}}{I_e} \\ &= \frac{5,5 \times 6,162237 \text{ mm}}{1} \\ &= 33,892 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_8 &= \frac{C_d \times \delta_{8e}}{I_e} \\ &= \frac{5,5 \times 7,208292 \text{ mm}}{1} \\ &= 39,6456 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_9 &= \frac{C_d \times \delta_{9e}}{I_e} \\ &= \frac{5,5 \times 6,10183 \text{ mm}}{1} \\ &= 33,560 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_9 &= \frac{C_d \times \delta_{9e}}{I_e} \\ &= \frac{5,5 \times 7,052887 \text{ mm}}{1} \\ &= 38,7909 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{10} &= \frac{C_d \times \delta_{10e}}{I_e} \\ &= \frac{5,5 \times 6,042182 \text{ mm}}{1} \\ &= 33,232 \text{ mm}\end{aligned}$$

$$\begin{aligned}\delta_{10} &= \frac{C_d \times \delta_{10e}}{I_e} \\ &= \frac{5,5 \times 1,749917 \text{ mm}}{1} \\ &= 6,995949 \text{ mm}\end{aligned}$$

**SNI 1726:2012 (Arah Y)**

$$\begin{aligned}\Delta_1 &\leq \Delta_{ijin} \\ 8,470 \text{ mm} &\leq 64,615 \text{ mm} \\ &\text{(Memenuhi Persyaratan)}\end{aligned}$$

**SNI 1726:2019 (Arah Y)**

$$\begin{aligned}\Delta_1 &\leq \Delta_{ijin} \\ 10,170 \text{ mm} &\leq 64,615 \text{ mm} \\ &\text{(Memenuhi Persyaratan)}\end{aligned}$$

$$\Delta_2 \leq \Delta_{ijin}$$

$$21,202 \text{ mm} \leq 64,615 \text{ mm}$$

(Memenuhi Persyaratan)

$$\Delta_3 \leq \Delta_{ijin}$$

$$30,033 \text{ mm} \leq 64,615 \text{ mm}$$

(Memenuhi Persyaratan)

$$\Delta_4 \leq \Delta_{ijin}$$

$$33,681 \text{ mm} \leq 52,308 \text{ mm}$$

(Memenuhi Persyaratan)

$$\Delta_5 \leq \Delta_{ijin}$$

$$31,223 \text{ mm} \leq 52,308 \text{ mm}$$

(Memenuhi Persyaratan)

$$\Delta_6 \leq \Delta_{ijin}$$

$$32,904 \text{ mm} \leq 52,308 \text{ mm}$$

(Memenuhi Persyaratan)

$$\Delta_7 \leq \Delta_{ijin}$$

$$33,746 \text{ mm} \leq 52,308 \text{ mm}$$

(Memenuhi Persyaratan)

$$\Delta_8 \leq \Delta_{ijin}$$

$$33,892 \text{ mm} \leq 52,308 \text{ mm}$$

(Memenuhi Persyaratan)

$$\Delta_9 \leq \Delta_{ijin}$$

$$33,560 \text{ mm} \leq 52,308 \text{ mm}$$

(Memenuhi Persyaratan)

$$\Delta_2 \leq \Delta_{ijin}$$

$$25,146 \text{ mm} \leq 64,615 \text{ mm}$$

(Memenuhi Persyaratan)

$$\Delta_3 \leq \Delta_{ijin}$$

$$35,662 \text{ mm} \leq 64,615 \text{ mm}$$

(Memenuhi Persyaratan)

$$\Delta_4 \leq \Delta_{ijin}$$

$$33,727 \text{ mm} \leq 52,308 \text{ mm}$$

(Memenuhi Persyaratan)

$$\Delta_5 \leq \Delta_{ijin}$$

$$36,909 \text{ mm} \leq 52,308 \text{ mm}$$

(Memenuhi Persyaratan)

$$\Delta_6 \leq \Delta_{ijin}$$

$$38,733 \text{ mm} \leq 52,308 \text{ mm}$$

(Memenuhi Persyaratan)

$$\Delta_7 \leq \Delta_{ijin}$$

$$39,553 \text{ mm} \leq 52,308 \text{ mm}$$

(Memenuhi Persyaratan)

$$\Delta_8 \leq \Delta_{ijin}$$

$$39,646 \text{ mm} \leq 52,308 \text{ mm}$$

(Memenuhi Persyaratan)

$$\Delta_9 \leq \Delta_{ijin}$$

$$38,791 \text{ mm} \leq 52,308 \text{ mm}$$

(Memenuhi Persyaratan)



$$\Delta_{10} \leq \Delta_{ijin}$$
$$33,232 \text{ mm} \leq 52,308 \text{ mm}$$

(Memenuhi Persyaratan)

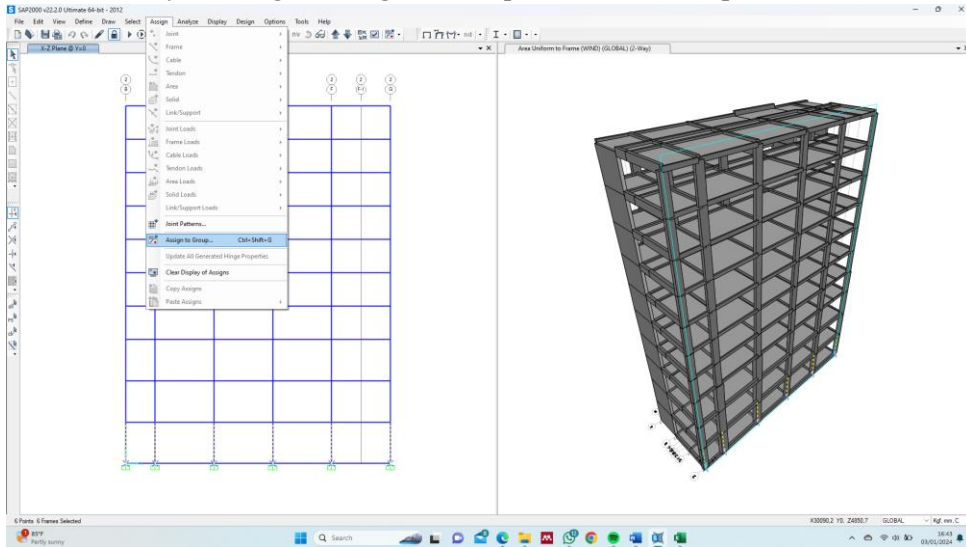
$$\Delta_{10} \leq \Delta_{ijin}$$
$$38,478 \text{ mm} \leq 52,308 \text{ mm}$$

(Memenuhi Persyaratan)

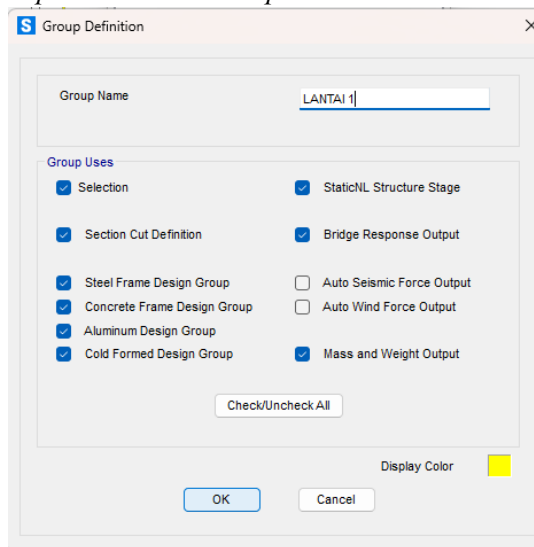
## LAMPIRAN III

### CARA MENAMPILKAN *OUTPUT P-DELTA*

Untuk mengetahui nilai P-Delta yang telah dianalisis pada *software* SAP2000 v.22.2.0, dapat dilakukan dengan cara klik seluruh kolom pada tiap tingkat beserta *joint* dibawahnya – *Assign – Assign to Group – Add New Group*.



Lalu klik *Define Groups – Add New Groups* – Definisikan Nama Grup – Ok.

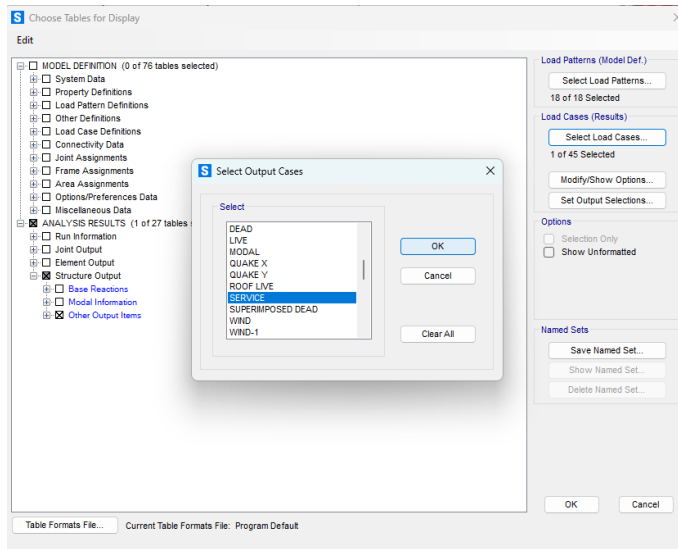


Lalu definisikan setiap grup yang telah dibuat ke dalam menu *Section Cut* dengan cara klik *Define – Section Cut – Add New Section Cut –* Masukkan grup yang telah didefinisikan sebelumnya. Ulangi di tiap tingkat lainnya.

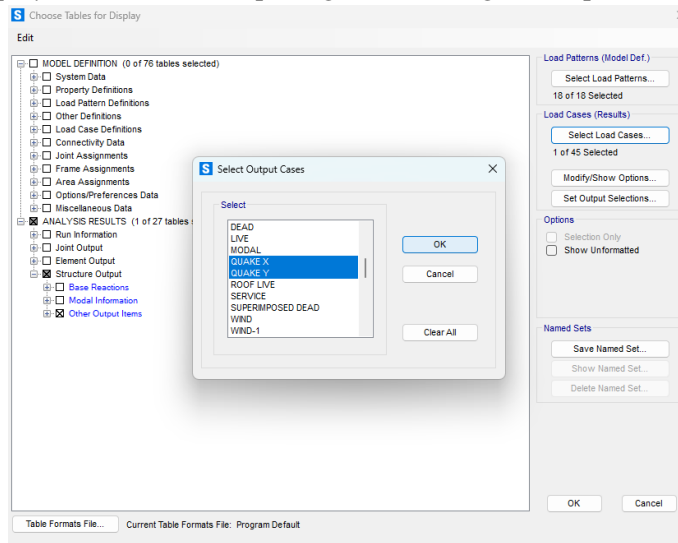
Selanjutnya membuat *Load Combinations* beban *services* dengan mengisi beban mati dan beban hidup yang dikombinasikan.

Load Case Name	Load Case Type	Mode	Scale Factor
LIVE	Linear Static		1
DEAD	Linear Static		1
LIVE	Linear Static		1

Lalu ekspor nilai *P* dari *Load Combination* tersebut dengan cara klik *Display – Show Tables – Other Output Items – Section Cut Forces*.



Lalu ekspor nilai *Quake X* dan *Quake Y* untuk memperoleh nilai  $V_x$  dan  $V_y$  dengan cara klik *Display – Show Tables – pilih Quake X dan Quake Y pada Load Case*.



## LAMPIRAN IV

### PERHITUNGAN P-DELTA ARAH X DAN Y

#### SNI 1726:2012 (Arah X)

$$\frac{P_x \times \Delta_x \times I_e}{V_x \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{35713,807 \text{ kN} \times 17,174 \text{ mm} \times 1,00}{739,617 \text{ kN} \times 4200 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,03590 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_x \times \Delta_x \times I_e}{V_x \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{31397,918 \text{ kN} \times 33,489 \text{ mm} \times 1,00}{700,351 \text{ kN} \times 4200 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,06499 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_x \times \Delta_x \times I_e}{V_x \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{27211,186 \text{ kN} \times 41,486 \text{ mm} \times 1,00}{703,184 \text{ kN} \times 4200 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,06950 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_x \times \Delta_x \times I_e}{V_x \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{23259,429 \text{ kN} \times 33,681 \text{ mm} \times 1,00}{785,904 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,05331 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_x \times \Delta_x \times I_e}{V_x \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{19448,531 \text{ kN} \times 34,232 \text{ mm} \times 1,00}{695,127 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,05122 \leq 0,090909$$

(Memenuhi Persyaratan)

#### SNI 1726:2019 (Arah X)

$$\frac{P_x \times \Delta_x \times I_e}{V_x \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{36321,801 \text{ kN} \times 20,592 \text{ mm} \times 1,00}{875,167 \text{ kN} \times 4200 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,03700 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_x \times \Delta_x \times I_e}{V_x \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{32005,17 \text{ kN} \times 40,278 \text{ mm} \times 1,00}{837,382 \text{ kN} \times 4200 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,06664 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_x \times \Delta_x \times I_e}{V_x \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{27817,119 \text{ kN} \times 49,883 \text{ mm} \times 1,00}{845,992 \text{ kN} \times 4200 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,07100 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_x \times \Delta_x \times I_e}{V_x \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{23874,857 \text{ kN} \times 40,470 \text{ mm} \times 1,00}{944,054 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,05473 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_x \times \Delta_x \times I_e}{V_x \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{20073,819 \text{ kN} \times 41,024 \text{ mm} \times 1,00}{831,641 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,05295 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_x \times \Delta_x \times I_e}{V_x \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{15701,453 \text{ kN} \times 32,852 \text{ mm} \times 1,00}{664,272 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,04153 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_x \times \Delta_x \times I_e}{V_x \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{12024,464 \text{ kN} \times 30,260 \text{ mm} \times 1,00}{612,315 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,03178 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_x \times \Delta_x \times I_e}{V_x \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{8356,835 \text{ kN} \times 27,662 \text{ mm} \times 1,00}{511,433 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,02417 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_x \times \Delta_x \times I_e}{V_x \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{4733,056 \text{ kN} \times 23,903 \text{ mm} \times 1,00}{452,46 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,01337 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_x \times \Delta_x \times I_e}{V_x \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{1157,944 \text{ kN} \times 19,127 \text{ mm} \times 1,00}{332,853 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,00356 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_x \times \Delta_x \times I_e}{V_x \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{16337,212 \text{ kN} \times 39,162 \text{ mm} \times 1,00}{788,84 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,04337 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_x \times \Delta_x \times I_e}{V_x \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{12671,617 \text{ kN} \times 35,762 \text{ mm} \times 1,00}{717,12 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,03379 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_x \times \Delta_x \times I_e}{V_x \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{9017,02 \text{ kN} \times 32,278 \text{ mm} \times 1,00}{587,512 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,02649 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_x \times \Delta_x \times I_e}{V_x \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{5408,452 \text{ kN} \times 27,383 \text{ mm} \times 1,00}{506,668 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,01563 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_x \times \Delta_x \times I_e}{V_x \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{1853,405 \text{ kN} \times 21,324 \text{ mm} \times 1,00}{350,889 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,00602 \leq 0,090909$$

(Memenuhi Persyaratan)

**SNI 1726:2012 (Arah Y)**

$$\frac{P_y \times \Delta_y \times I_e}{V_y \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{35713,807 \text{ kN} \times 8,470 \text{ mm} \times 1,00}{153,123 \text{ kN} \times 4200 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,08552 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_y \times \Delta_y \times I_e}{V_y \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{31397,918 \text{ kN} \times 21,202 \text{ mm} \times 1,00}{289,98 \text{ kN} \times 4200 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,09938 \leq 0,090909$$

(Tidak Memenuhi Persyaratan)

$$\frac{P_y \times \Delta_y \times I_e}{V_y \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{27211,186 \text{ kN} \times 30,033 \text{ mm} \times 1,00}{357,423 \text{ kN} \times 4200 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,09898 \leq 0,090909$$

(Tidak Memenuhi Persyaratan)

$$\frac{P_y \times \Delta_y \times I_e}{V_y \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{23259,429 \text{ kN} \times 28,604 \text{ mm} \times 1,00}{468,092 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,07601 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_y \times \Delta_y \times I_e}{V_y \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{19448,531 \text{ kN} \times 31,223 \text{ mm} \times 1,00}{473,19 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,06863 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_y \times \Delta_y \times I_e}{V_y \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{15701,453 \text{ kN} \times 32,904 \text{ mm} \times 1,00}{379,1 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,07288 \leq 0,090909$$

(Memenuhi Persyaratan)

**SNI 1726:2019 (Arah Y)**

$$\frac{P_y \times \Delta_y \times I_e}{V_y \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{36321,801 \text{ kN} \times 10,170 \text{ mm} \times 1,00}{186,591 \text{ kN} \times 4200 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,08570 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_y \times \Delta_y \times I_e}{V_y \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{32005,17 \text{ kN} \times 25,146 \text{ mm} \times 1,00}{349,625 \text{ kN} \times 4200 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,09965 \leq 0,090909$$

(Tidak Memenuhi Persyaratan)

$$\frac{P_y \times \Delta_y \times I_e}{V_y \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{27817,119 \text{ kN} \times 35,662 \text{ mm} \times 1,00}{433,768 \text{ kN} \times 4200 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,09900 \leq 0,090909$$

(Tidak Memenuhi Persyaratan)

$$\frac{P_y \times \Delta_y \times I_e}{V_y \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{23874,857 \text{ kN} \times 33,727 \text{ mm} \times 1,00}{551,268 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,07811 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_y \times \Delta_y \times I_e}{V_y \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{20073,819 \text{ kN} \times 36,909 \text{ mm} \times 1,00}{555,841 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,07128 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_y \times \Delta_y \times I_e}{V_y \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{16337,212 \text{ kN} \times 38,733 \text{ mm} \times 1,00}{442,865 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,07641 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_y \times \Delta_y \times I_e}{V_y \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{12024,464 \text{ kN} \times 33,746 \text{ mm} \times 1,00}{383,96 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,05651 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_y \times \Delta_y \times I_e}{V_y \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{8356,835 \text{ kN} \times 33,892 \text{ mm} \times 1,00}{353,065 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,04290 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_y \times \Delta_y \times I_e}{V_y \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{4733,056 \text{ kN} \times 33,560 \text{ mm} \times 1,00}{356,672 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,02382 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_y \times \Delta_y \times I_e}{V_y \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{1157,944 \text{ kN} \times 33,232 \text{ mm} \times 1,00}{209,658 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,00982 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_y \times \Delta_y \times I_e}{V_y \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{12671,617 \text{ kN} \times 39,553 \text{ mm} \times 1,00}{444,96 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,06023 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_y \times \Delta_y \times I_e}{V_y \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{9017,02 \text{ kN} \times 39,646 \text{ mm} \times 1,00}{405,038 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,04720 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_y \times \Delta_y \times I_e}{V_y \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{5408,452 \text{ kN} \times 38,791 \text{ mm} \times 1,00}{404,989 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,02770 \leq 0,090909$$

(Memenuhi Persyaratan)

$$\frac{P_y \times \Delta_y \times I_e}{V_y \times h_{sx} \times C_d} \leq \theta_{max}$$

$$\frac{1853,405 \text{ kN} \times 9,625 \text{ mm} \times 1,00}{234,392 \text{ kN} \times 3400 \text{ mm} \times 5,5} \leq 0,090909$$

$$0,01627 \leq 0,090909$$

(Memenuhi Persyaratan)

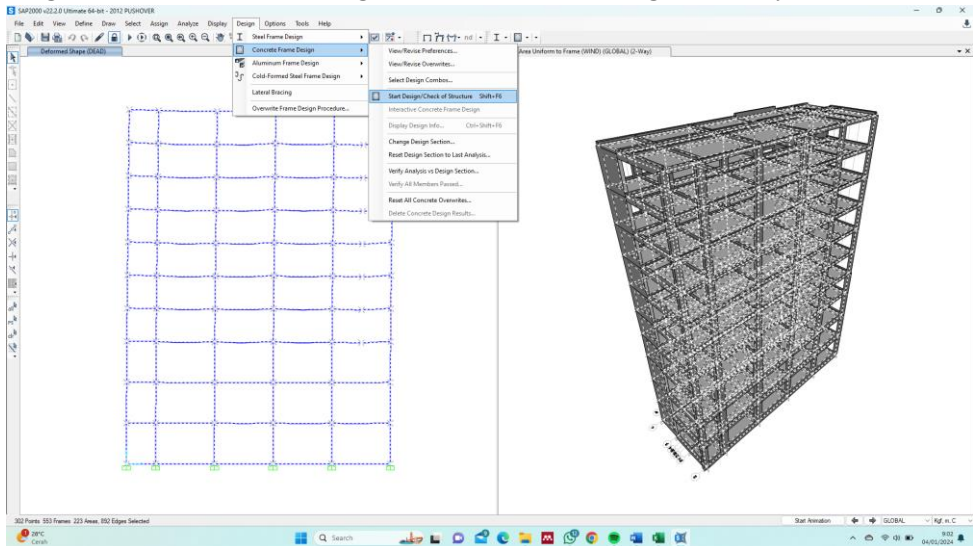


## LAMPIRAN V

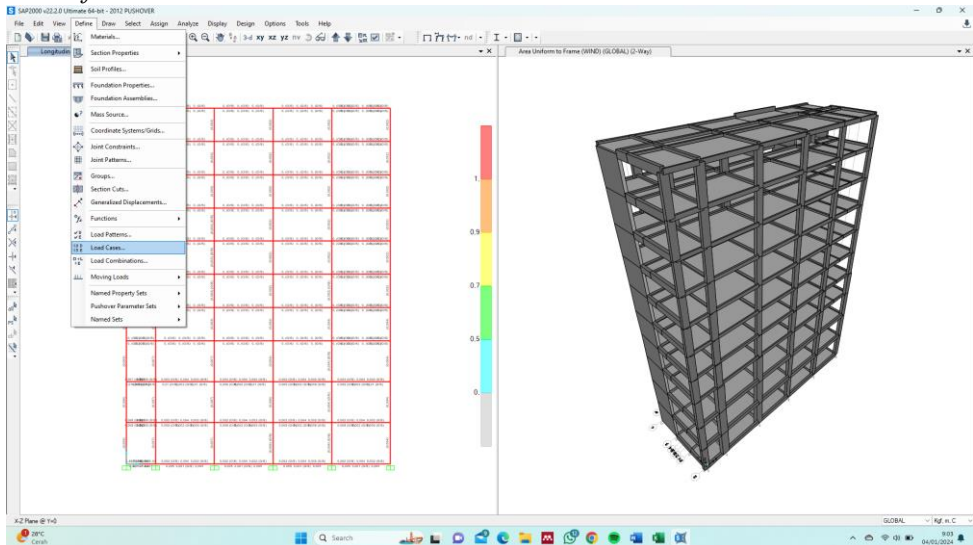
### CARA PEMBUATAN *HINGES* PADA ANALISA *PUSHOVER*

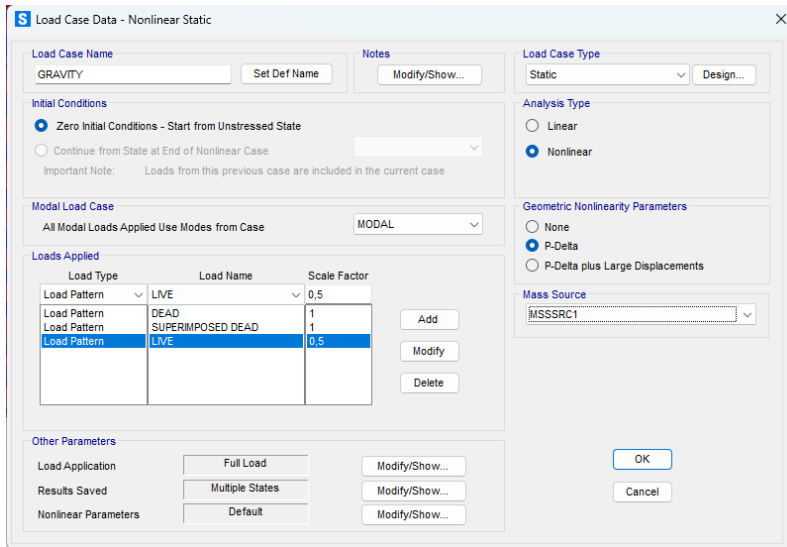
#### Langkah-1: Membuat Load Cases

Cek permodelan struktur yang sudah dirunning sebelumnya, blok semua *frame*, klik *Design – Concrete Frame Design – Start Concrete Design/Check of Structure*.

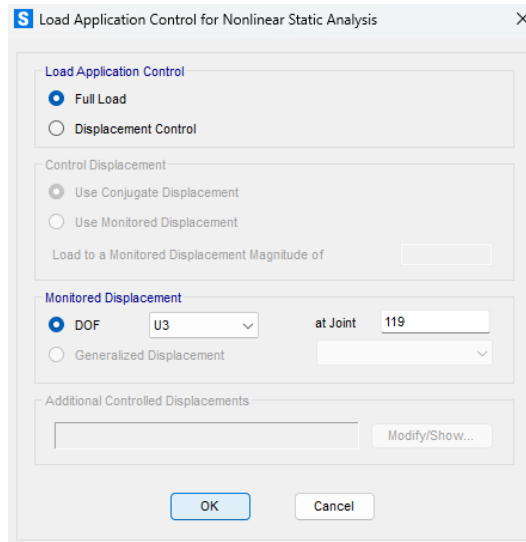


Klik *Define – Load Cases – Add New Load Case*.

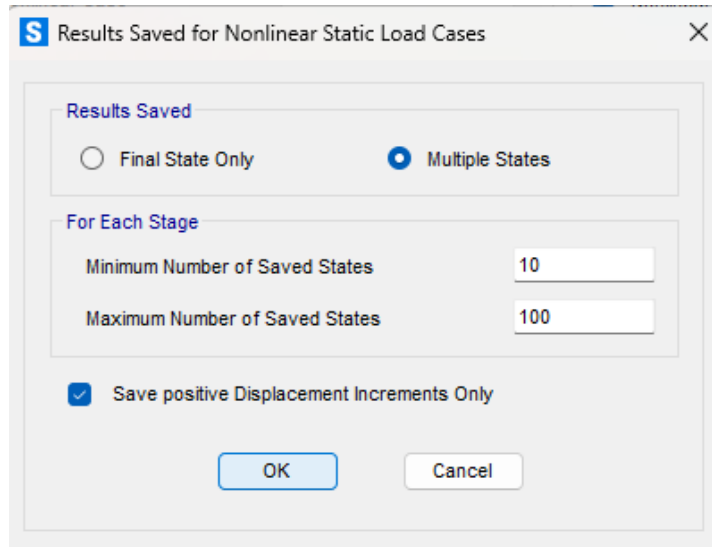




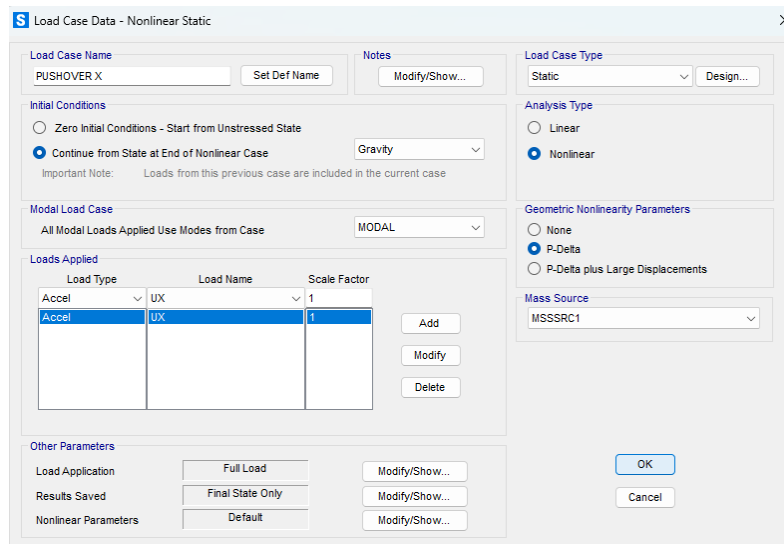
Isikan *Load Application* sesuai gambar, dikarenakan gravitasi merupakan beban arah z maka  $U_3 = U_Z$ .



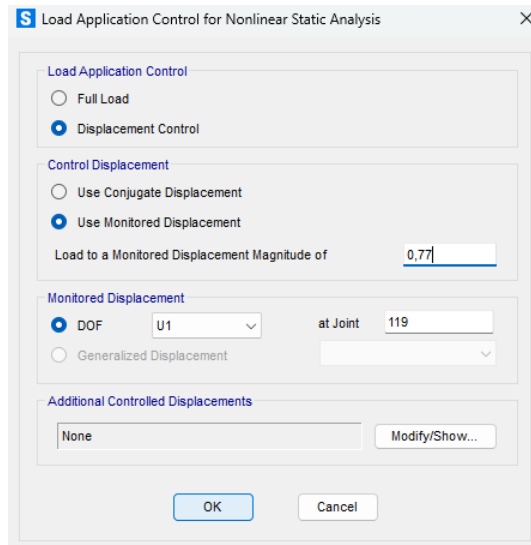
Ganti *Result Saved* menjadi *Multiple States*



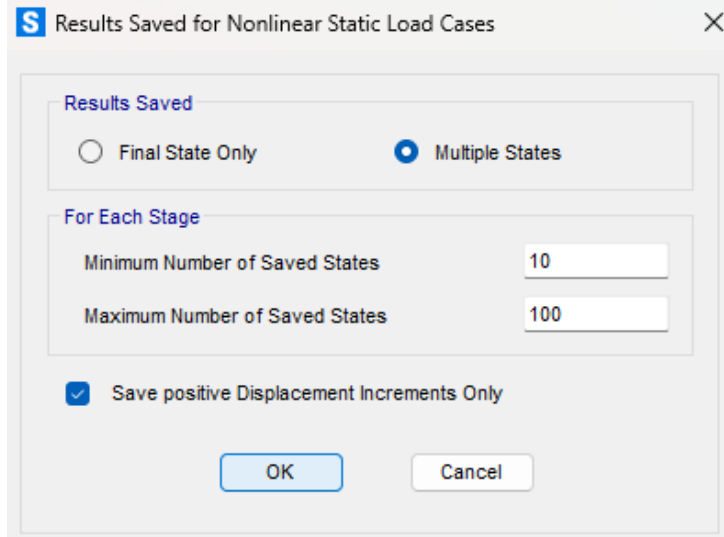
Selanjutnya, buat *pushover* untuk arah X dengan cara klik *Define – Load Cases – Add New Load Case*.



Klik *Modify/Show* pada *Load Application* lalu ganti nilai DOF U1 = UX.



Klik *Modify/Show* pada *Results Saved* dan ganti menjadi *Multiple States*.



Buat juga *pushover* arah y dengan cara klik *Define – Load Cases – Add New Load Case* lalu ganti nilai DOF pada *Load Application*  $U2 = UY$ .

**S Load Case Data - Nonlinear Static**

Load Case Name: PUSHOVERY    Set Def Name    Notes: Modify/Show...

Load Case Type: Static    Design...

**Initial Conditions**

Zero Initial Conditions - Start from Unstressed State

Continue from State at End of Nonlinear Case    GRAVITY

Important Note: Loads from this previous case are included in the current case

**Modal Load Case**

All Modal Loads Applied Use Modes from Case: MODAL

**Loads Applied**

Load Type	Load Name	Scale Factor
Accel	UY	1

Add    Modify    Delete

**Analysis Type**

Linear

Nonlinear

**Geometric Nonlinearity Parameters**

None

P-Delta

P-Delta plus Large Displacements

Mass Source: MSSSRC1

**Other Parameters**

Load Application: Full Load    Modify/Show...

Results Saved: Final State Only    Modify/Show...

Nonlinear Parameters: Default    Modify/Show...

OK    Cancel

Klik *Modify/Show* pada *Load Application* lalu ganti nilai DOF U2 = UY.

**S Load Application Control for Nonlinear Static Analysis**

**Load Application Control**

Full Load

Displacement Control

**Control Displacement**

Use Conjugate Displacement

Use Monitored Displacement

Load to a Monitored Displacement Magnitude of: 0,77

**Monitored Displacement**

DOF: U2 at Joint: 119

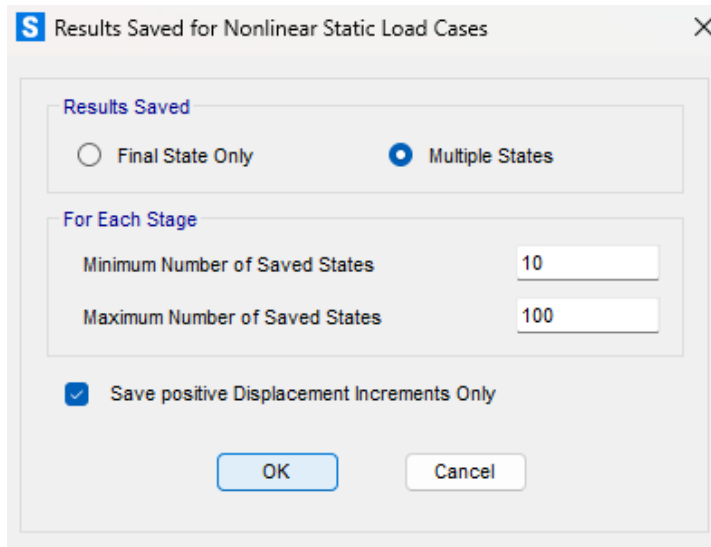
Generalized Displacement

**Additional Controlled Displacements**

None    Modify/Show...

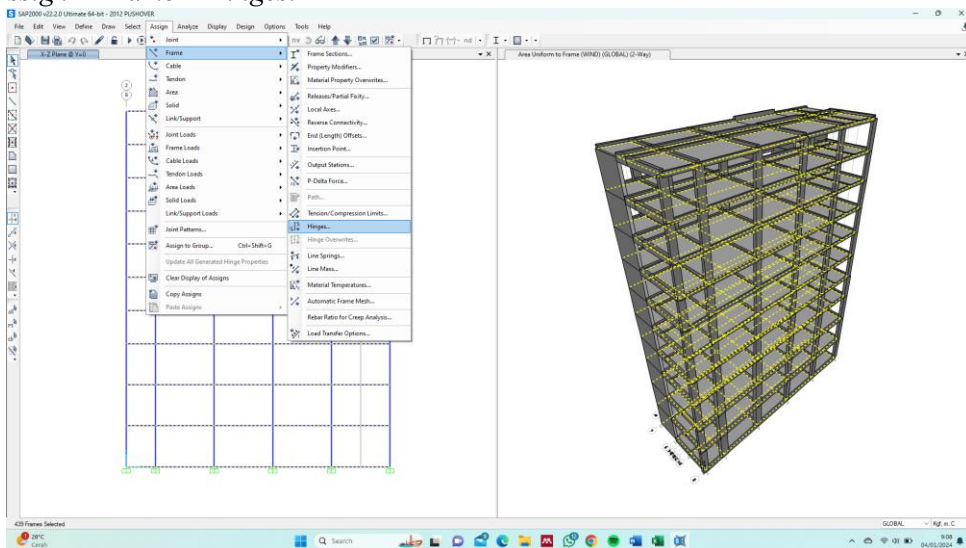
OK    Cancel

Klik *Modify/Show* pada *Results Saved* dan ganti menjadi *Multiple States*.



### Langkah-2: Membuat Hinges

Klik *Select – Properties – Frame Sections* – pilih semua balok – *Select* kemudian klik *Assign – Frame – Hinges*.



Perlu diketahui nilai *Relative Distance Frame Hinges* sebesar 0,1 dan 0,9 untuk masing-masing *pushover* arah X dan arah Y.

**S Assign Frame Hinges**

Frame Hinge Assignment Data

Hinge Property	Location Type	Relative Distance	Absolute Distance m
Auto	Relative To Clear Length	0.9	
Auto M3	Relative To Clear Length	0.1	
Auto M3	Relative To Clear Length	0.9	

Add Hinge...  
Modify Hinge...  
Note: Hold the Ctrl key down when clicking the Modify button to Modify or Show the Auto hinge properties of the selected hinge  
Delete Hinge

**Current Hinge Information**  
Type: From Tables In ASCE 41-13  
Table: Table 10-7 (Concrete Beams - Flexure) Item i  
DOF: M3

**Options**

Add Specified Hinge Assigns to Existing Hinge Assigns  
 Replace Existing Hinge Assigns with Specified Hinge Assigns

**Existing Hinge Assignments on Currently Selected Frame Objects**  
Number of Selected Frame Objects: 1342  
Total Number of Hinges on All Selected Frame Objects: 2684  
All 2684 existing hinge assignments will be removed when the above hinge assignment is applied

Fill Form with Hinges on Selected Frame Object

OK Close Apply

**S Auto Hinge Assignment Data**

Auto Hinge Type  
From Tables In ASCE 41-13

Select a Hinge Table  
Table 10-7 (Concrete Beams - Flexure) Item i

**Degree of Freedom**  
 M2  
 M3

**V Value From**  
 Case/Combo PUSHOVER X  
 User Value V2

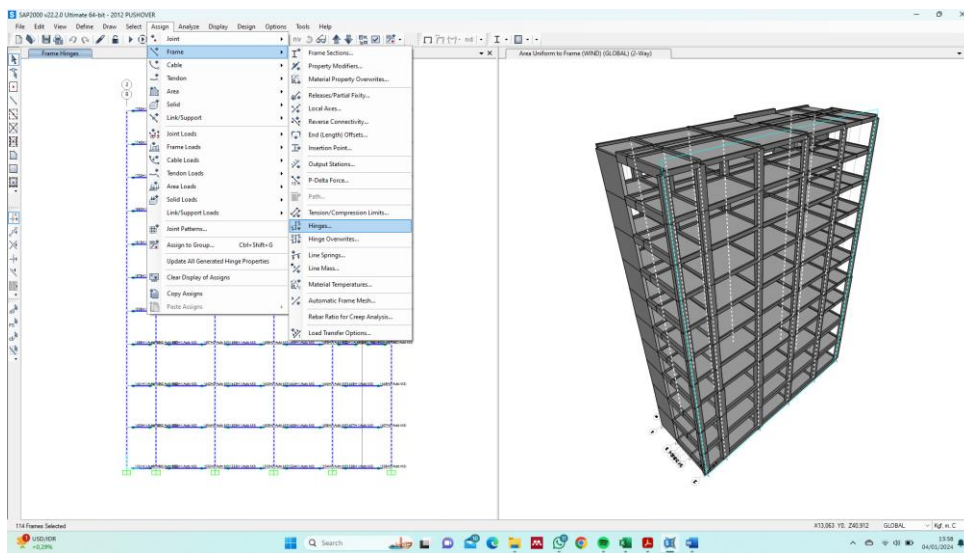
**Transverse Reinforcing**  
 Transverse Reinforcing is Conforming

**Reinforcing Ratio (p - p') / pbalanced**  
 From Current Design  
 User Value (for positive bending)

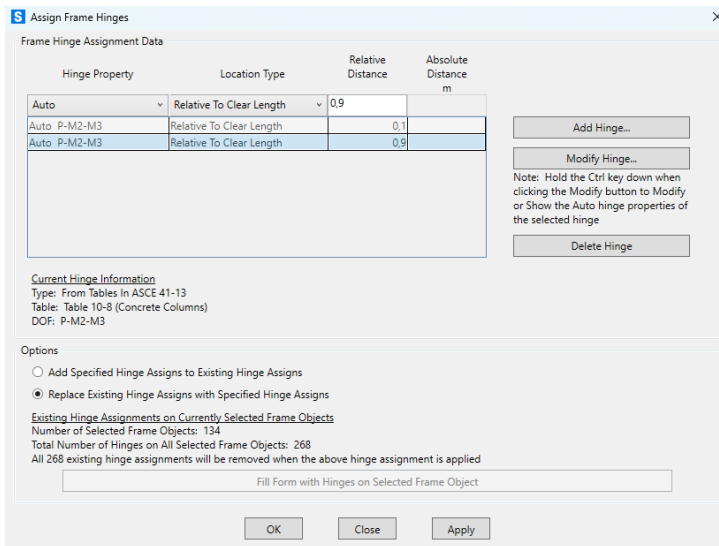
**Deformation Controlled Hinge Load Carrying Capacity**  
 Drops Load After Point E  
 Is Extrapolated After Point E

OK Cancel

Klik *Select – Properties – Frame Sections* – pilih semua kolom – *Select* kemudian klik *Assign – Frame – Hinges*.



Perlu diketahui nilai *Relative Distance Frame Hinges* sebesar 0,1 dan 0,9 untuk masing-masing *pushover* arah X dan arah Y.





**S** Auto Hinge Assignment Data

Auto Hinge Type  
From Tables In ASCE 41-13

Select a Hinge Table  
Table 10-8 (Concrete Columns)

Degree of Freedom  
 M2     P-M2     Parametric P-M2-M3  
 M3         P-M3  
 M2-M3     P-M2-M3

Concrete Column Failure Condition  
 Condition I - Flexure     Condition IV - Development  
 Condition II - Flexure/Shear  
 Condition III - Shear

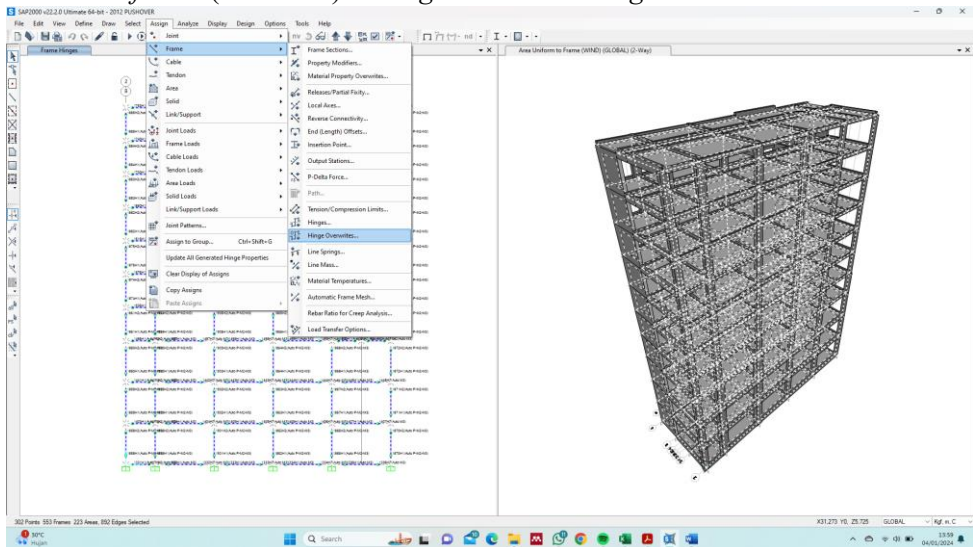
Deformation Controlled Hinge Load Carrying Capacity  
 Drops Load After Point E  
 Is Extrapolated After Point E

P and V Values From  
 Case/Combo    PUSHOVER X  
 User Value  
V2:     V3:

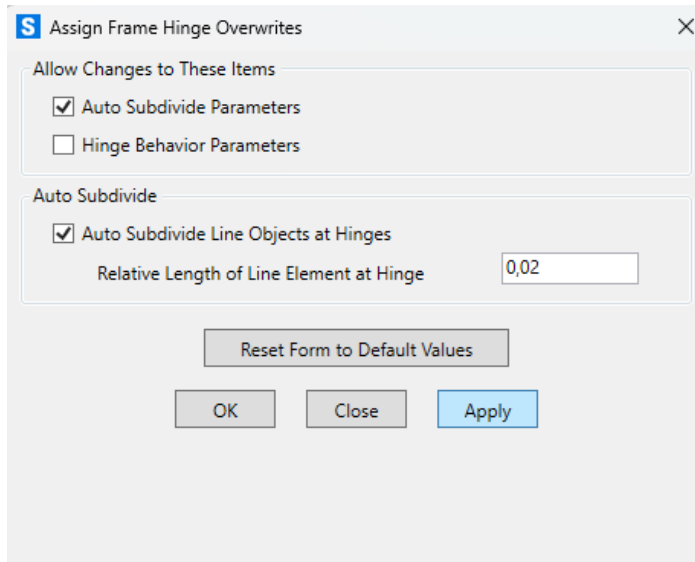
Shear Reinforcing Ratio  $p = A_v / (b_w * s)$   
 From Current Design  
 User Value   

OK    Cancel

Klik semua *frame* (CTRL+A) – Assign – Frame – Hinges Overwrites.

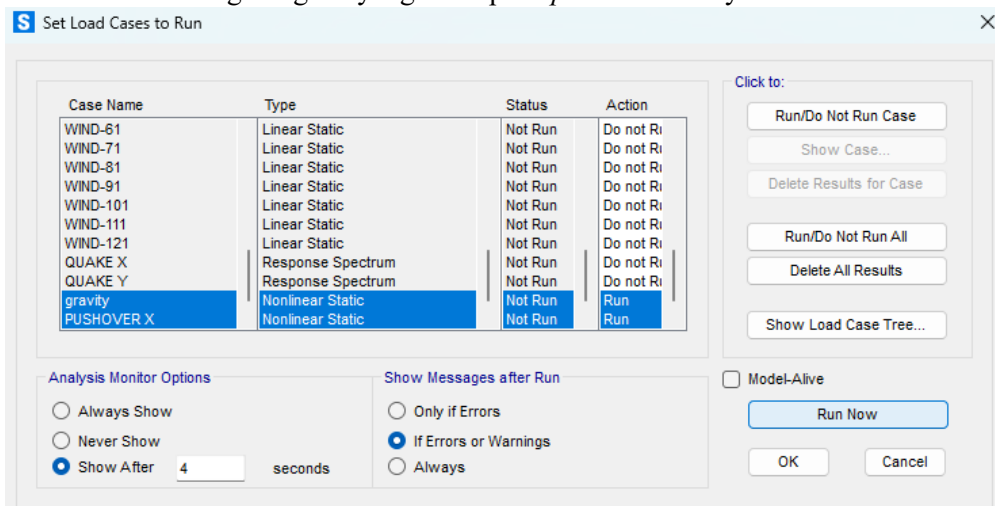


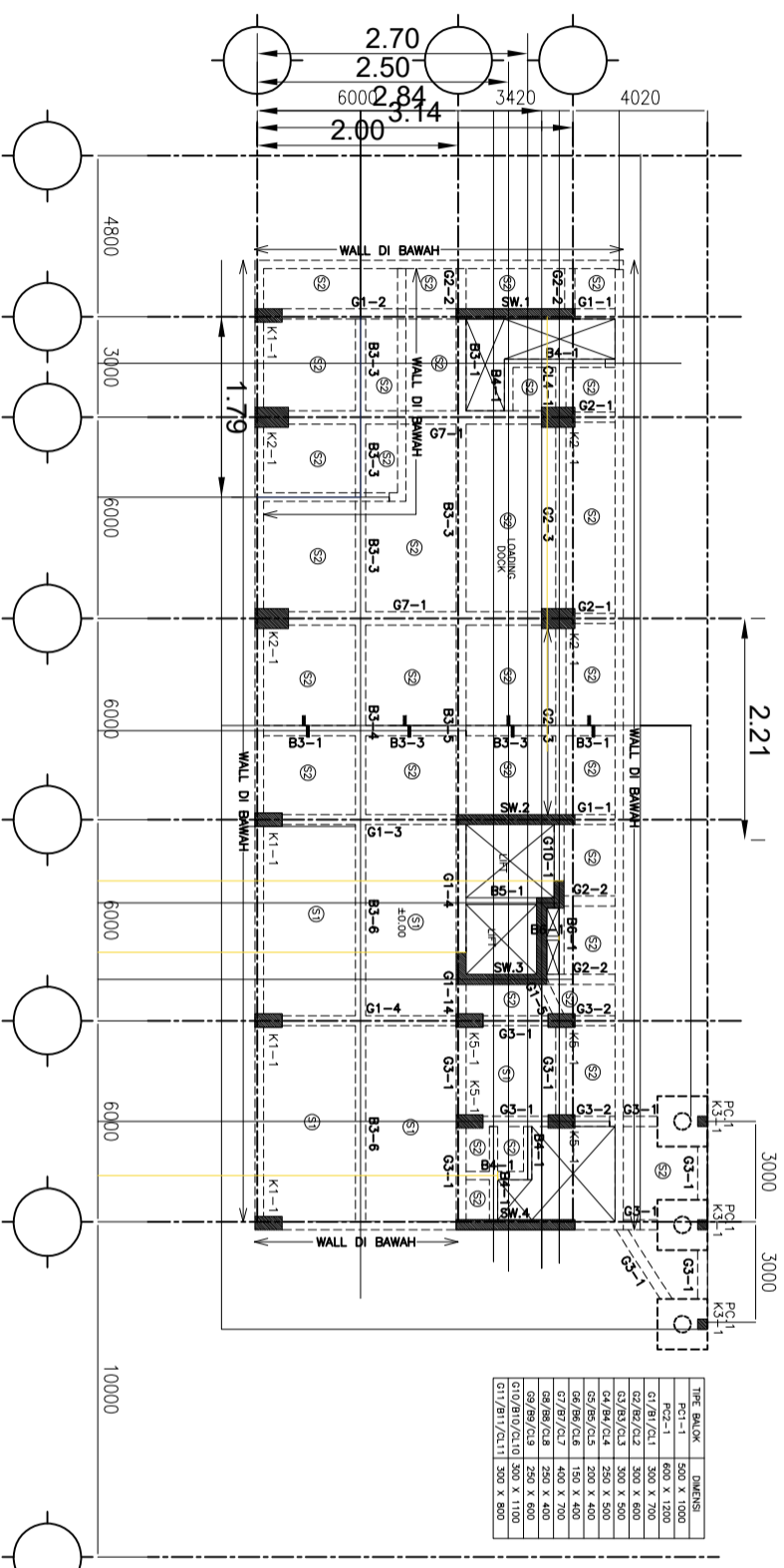
Checklist Auto Subdivide Line Objective at Hinges – Unchecklist Hinge Behavior.



### **Langkah-3: Run Analysis**

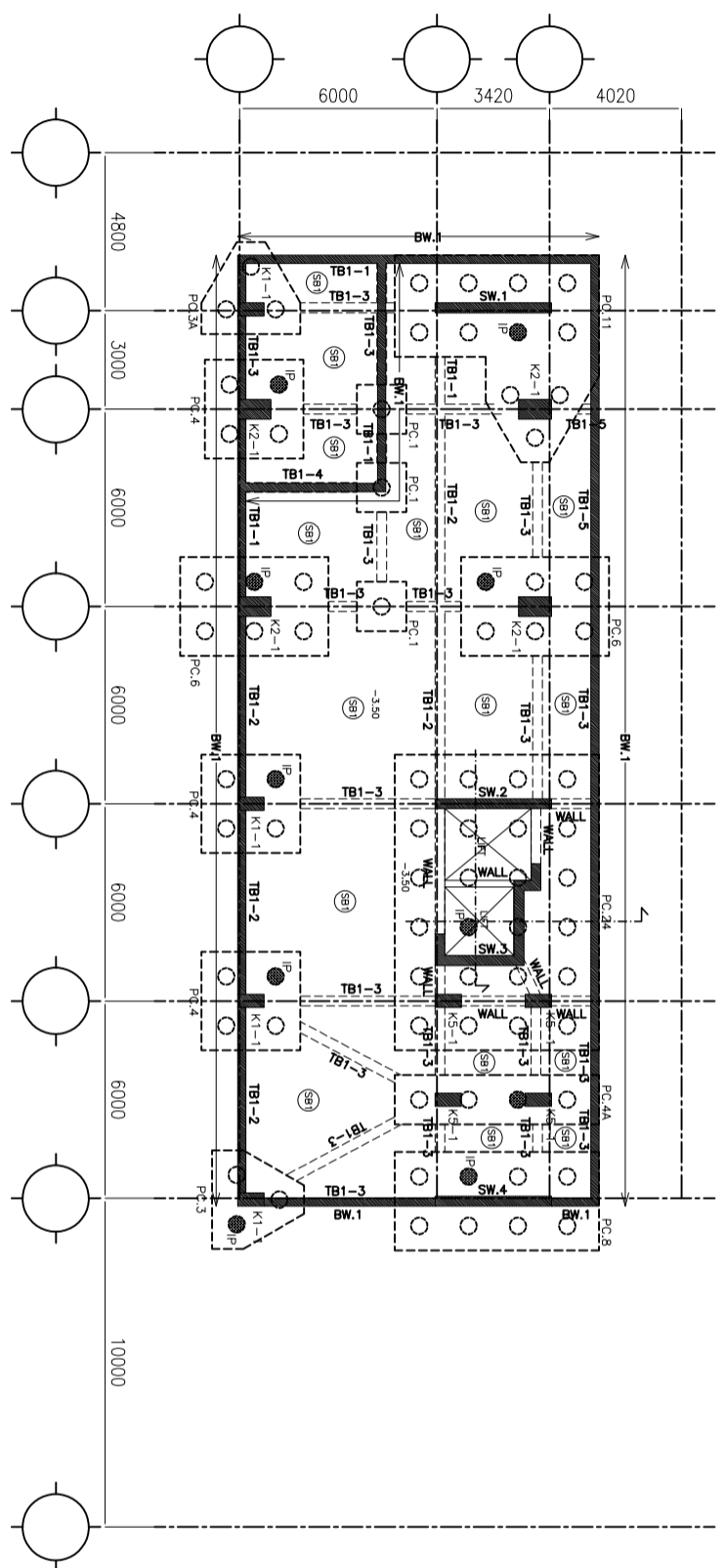
Jika semua langkah telah dilakukan, klik *Analyze – Run Analysis* – pilih *pushover* arah *x* – *Run Now*. Ulangi langkah yang sama pada *pushover* arah *y*.





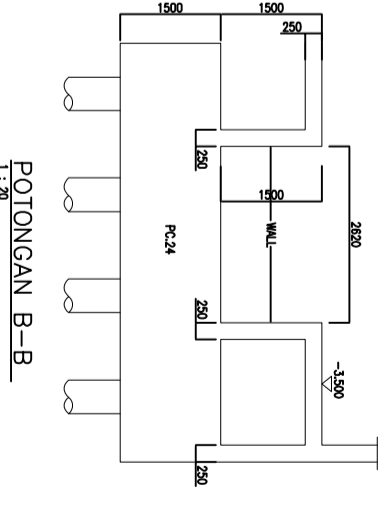
Tipe Balok	Dimensi
PC-1	500 x 1000
PC-2	600 x 1200
PC-3	500 x 700
PC-4	500 x 600
PC-5	500 x 500
PC-6	200 x 400
PC-7	250 x 400
PC-8	250 x 400
PC-9	250 x 600
PC-10	500 x 1100
PC-11	500 x 800

SKALA 1 : 100

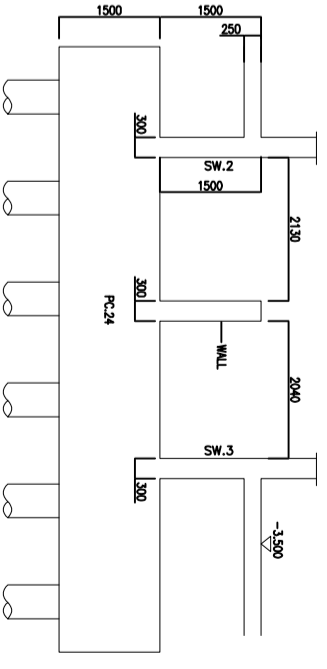


SKALA 1 : 100

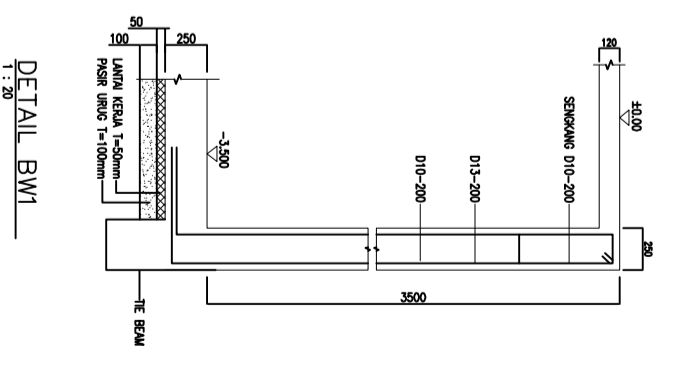
● = INDIKATOR PILE



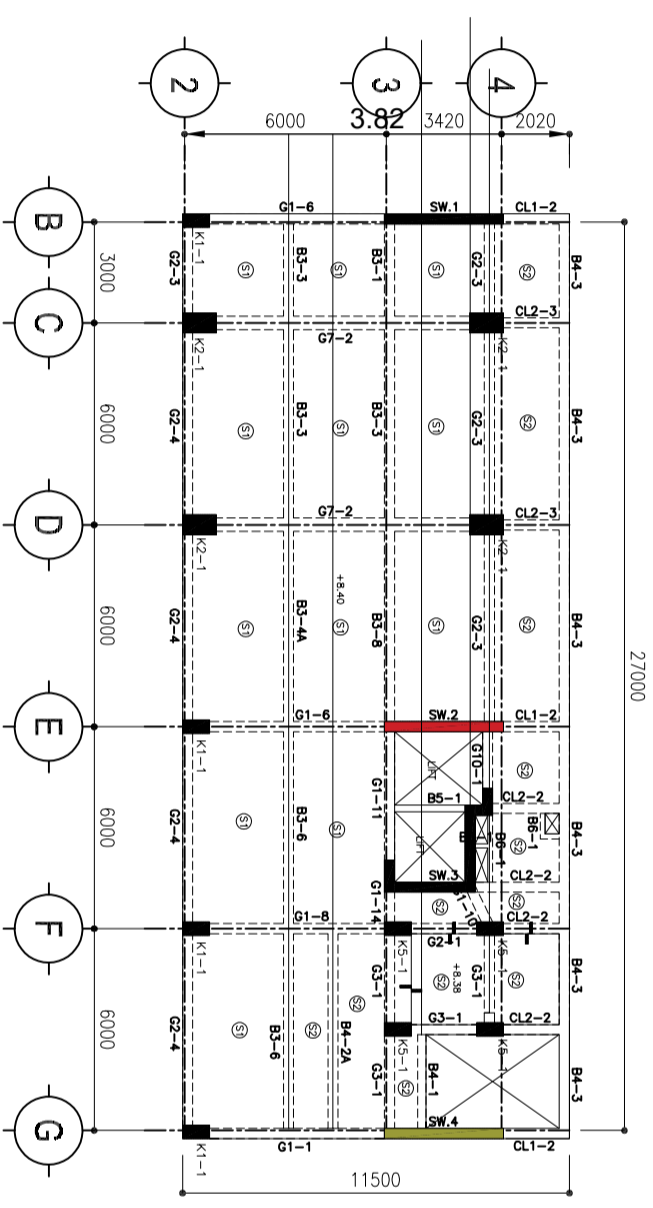
POTONGAN A-A  
1 : 20



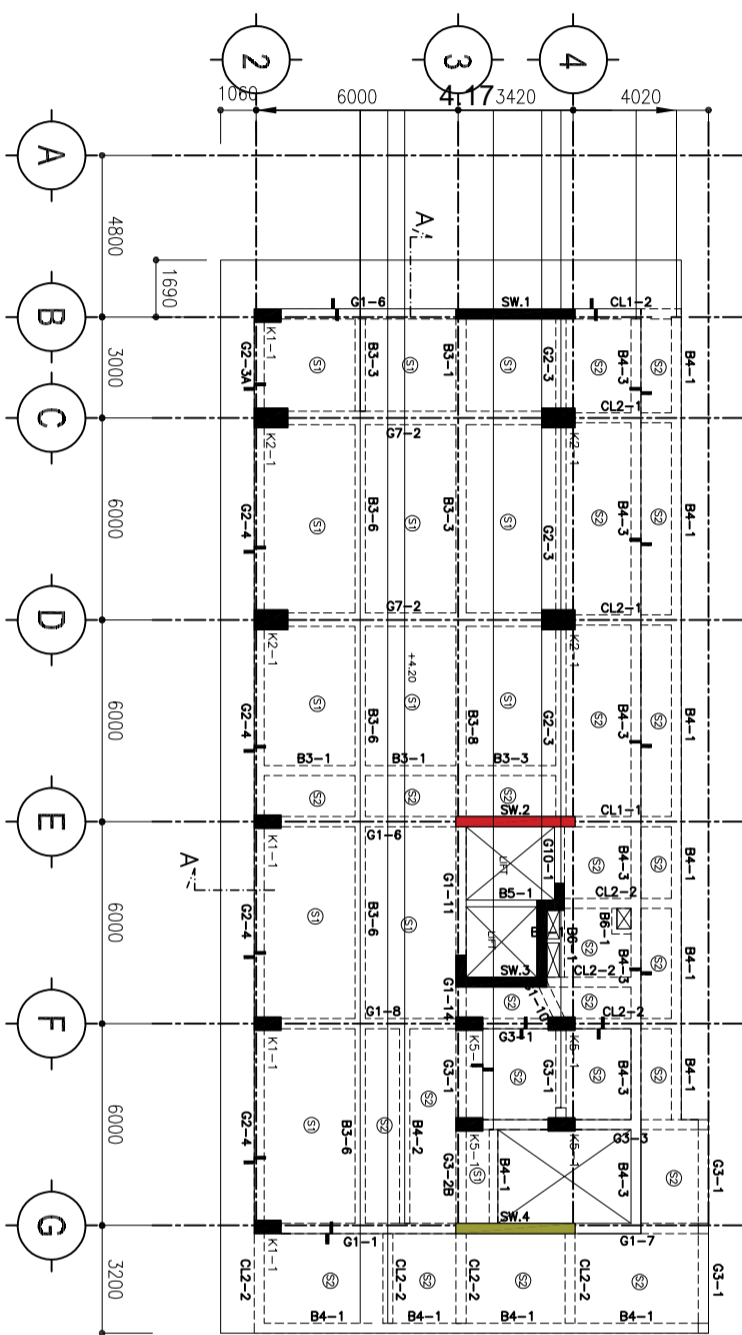
POTONGAN B-B  
1 : 20



DETAIL B-W1  
1 : 20

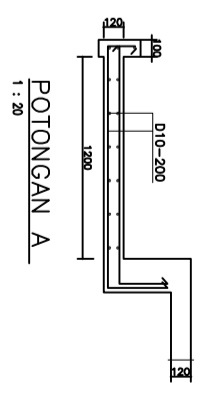


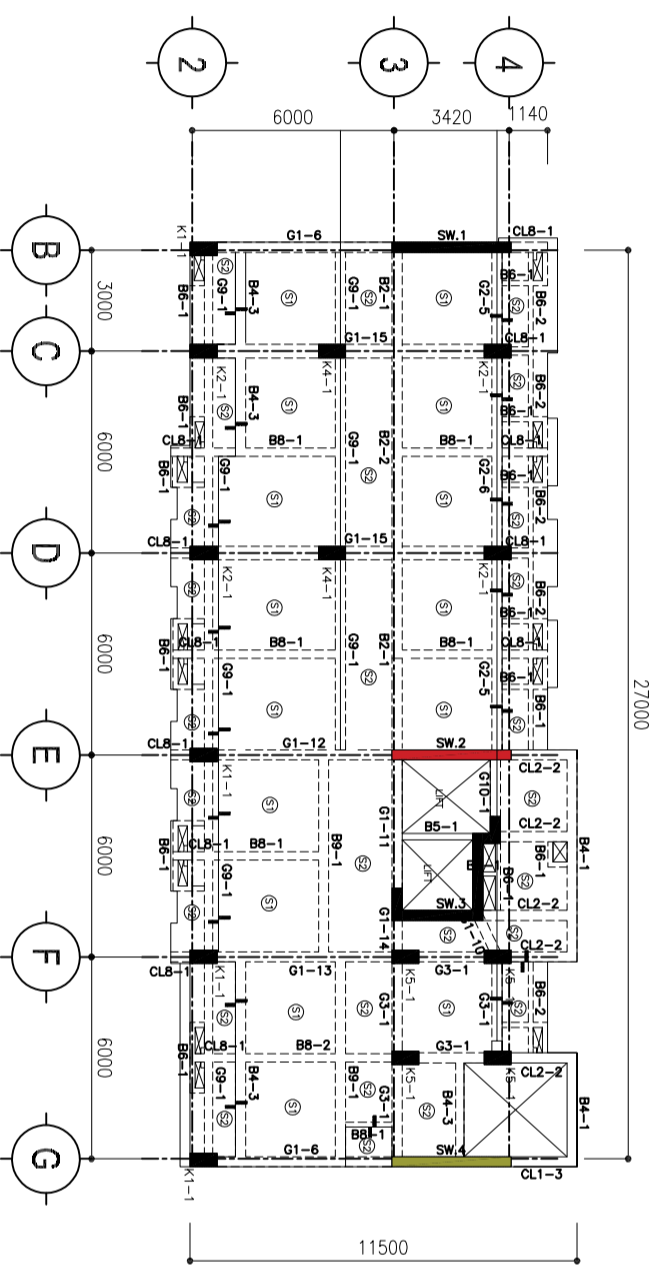
DENAH LANTAI 3  
SKALA 1 : 100



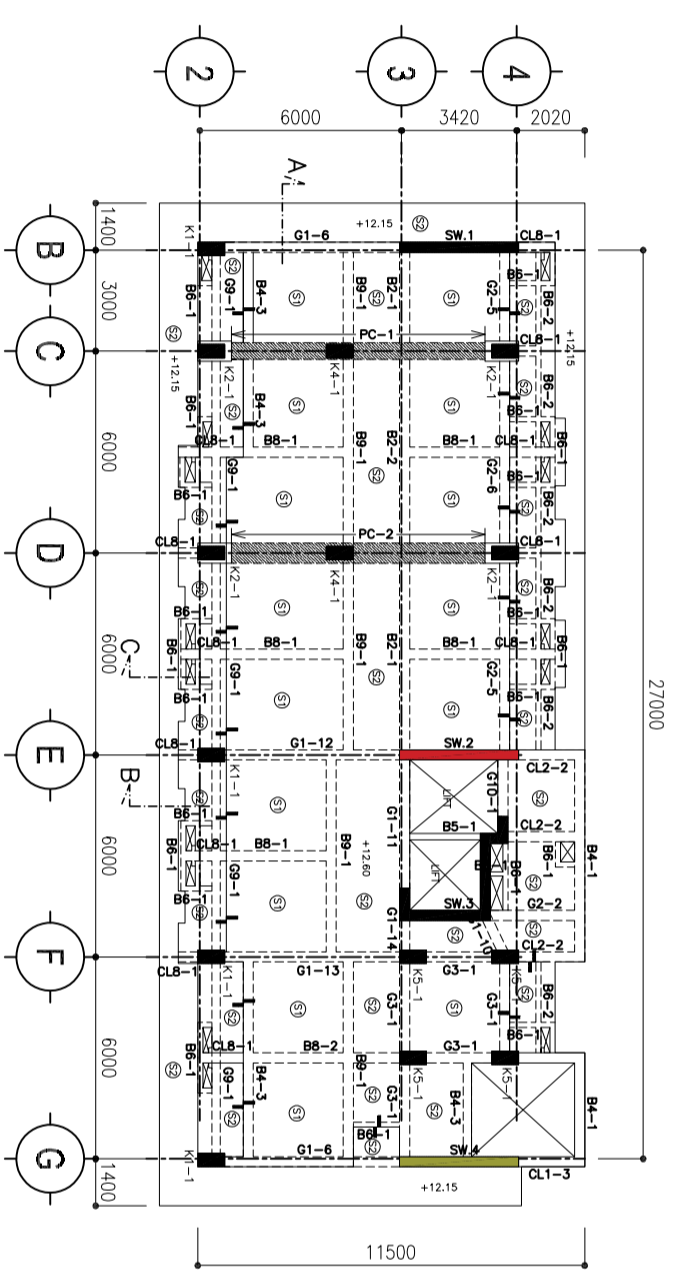
DENAH LANTAI 2  
SKALA 1 : 100

Tipe Balok	Dimensi
RC-1	500 x 500
RC-2	600 x 1200
G1/B1/C1	500 x 700
G2/B2/C2	500 x 600
G3/B3/C3	500 x 500
G4/B4/C4	200 x 500
G5/B5/C5	200 x 400
G6/B6/C6	150 x 400
G7/B7/C7	400 x 700
G8/B8/C8	500 x 800
G9/B9/C9	500 x 800
G10/B10/C10	500 x 1100
G11/B11/C11	500 x 800



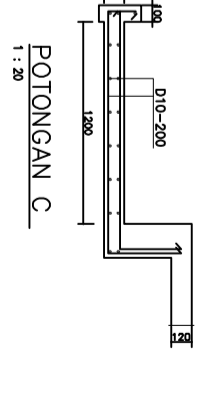
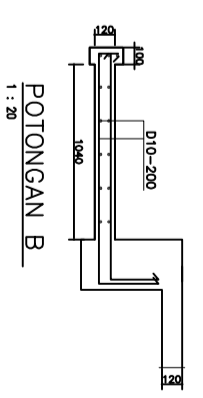
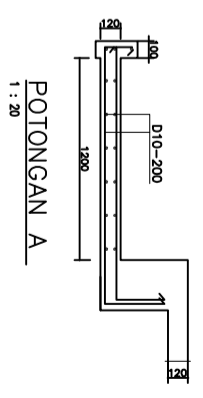


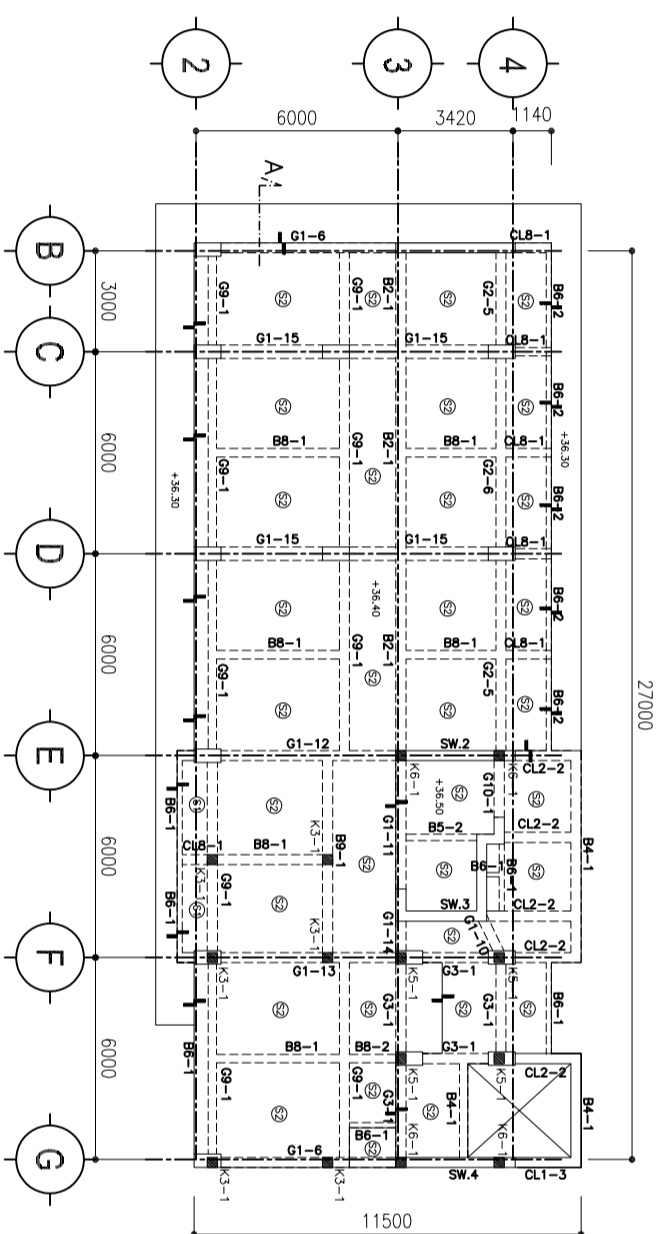
DENAH LANTAI 5-10  
SKALA 1 : 100



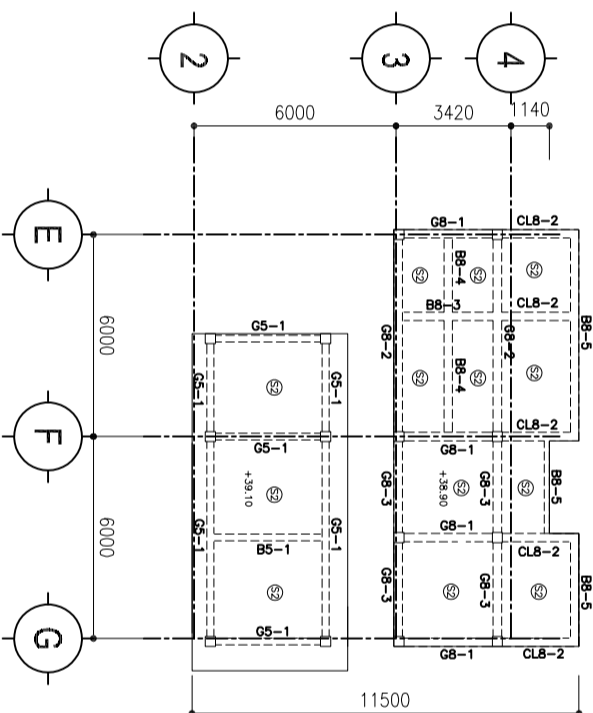
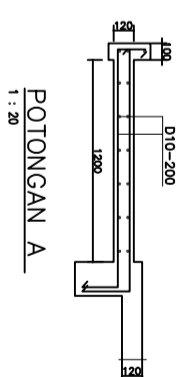
DENAH LANTAI 4  
SKALA 1 : 100

THE BLOCK	DIMENSI
P1-1	500 X 1000
G1/B1/C1	500 X 700
G2/B2/C2	500 X 600
G3/B3/C3	500 X 500
G4/B4/C4	250 X 500
G5/B5/C5	200 X 400
G6/B6/C6	150 X 400
G7/B7/C7	400 X 700
G8/B8/C8	250 X 400
G9/B9/C9	250 X 600
G10/B10/C10	500 X 600
G11/B11/C11	500 X 800





DENAH DAK ATAP  
SKALA 1 : 100



DENAH ATAP MESIN LIFT  
SKALA 1 : 100

Tipe Balok	Dimensi
P-1	500 X 1000
P-2	500 X 400
G1/B1/C1	500 X 700
G2/B2/C2	500 X 600
G3/B3/C3	500 X 500
G4/B4/C4	250 X 500
G5/B5/C5	200 X 400
G6/B6/C6	150 X 400
G7/B7/C7	400 X 700
G8/B8/C8	250 X 400
G9/B9/C9	500 X 400
G10/B10/C10	500 X 1100
G11/B11/C11	500 X 600

KOLOM LEVEL	K1-1
DAK ATAP	
LANTAI 7	
DIMENSI	300 x 700
TULANGAN UTAMA	12 D16
SENGKANG	D10-100 + 1 KAPT D10-100
MUTU	K-300

KOLOM LEVEL	K2-1
DAK ATAP	
LANTAI 5	
DIMENSI	300 x 800
TULANGAN UTAMA	16 D16
SENGKANG	D10-100 + 1 KAPT D10-100
MUTU	K-300

KOLOM LEVEL	K4-1
DAK ATAP	
LANTAI 5	
DIMENSI	300 x 800
TULANGAN UTAMA	16 D16
SENGKANG	D10-100 + 1 KAPT D10-100
MUTU	K-300

KOLOM LEVEL	K5-1
ATAP	
DAK ATAP	
DIMENSI	300 x 300
TULANGAN UTAMA	12 D13
SENGKANG	D10-100
MUTU	K-300

KOLOM LEVEL	K6-1
ATAP	
DAK ATAP	
DIMENSI	300 x 300
TULANGAN UTAMA	12 D13
SENGKANG	D10-100
MUTU	K-300

LANTAI 7	
LANTAI 5	
DIMENSI	300 x 800
TULANGAN UTAMA	12 D16
SENGKANG	D10-100 + 1 KAPT D10-100
MUTU	K-300

LANTAI 5	
LANTAI 4	
DIMENSI	400 x 800
TULANGAN UTAMA	16 D16
SENGKANG	D10-100 + 1 KAPT D10-100
MUTU	K-400

LANTAI 5	
LANTAI 4	
DIMENSI	300 x 800
TULANGAN UTAMA	16 D16
SENGKANG	D10-100 + 2 KAPT D10-100
MUTU	K-400

DAK ATAP	
LANTAI 7	
DIMENSI	300 x 700
TULANGAN UTAMA	12 D16
SENGKANG	D10-100 + 1 KAPT D10-100
MUTU	K-300

KOLOM LEVEL	K7-1
LANTAI 1	
BASEMENT	
DIMENSI	400 x 400
TULANGAN UTAMA	8 D16
SENGKANG	D10-100
MUTU	K-400

LANTAI 5	
BASEMENT	
DIMENSI	400 x 800
TULANGAN UTAMA	18 D16
SENGKANG	D10-100 + 1 KAPT D10-100
MUTU	K-400

LANTAI 4	
BASEMENT	
DIMENSI	600 x 1000
TULANGAN UTAMA	26 D19
SENGKANG	D10-100 + 3 KAPT D10-100
MUTU	K-400

KOLOM LEVEL	K3-1
LANTAI 2	
LANTAI 1	
DIMENSI	300 x 300
TULANGAN UTAMA	8 D13
SENGKANG	D10-100
MUTU	K-300

LANTAI 7	
LANTAI 5	
DIMENSI	300 x 800
TULANGAN UTAMA	12 D16
SENGKANG	D10-100 + 1 KAPT D10-100
MUTU	K-300

KOLOM LEVEL	K7-1
LANTAI 1	
BASEMENT	
DIMENSI	400 x 800
TULANGAN UTAMA	18 D16
SENGKANG	D10-100 + 2 KAPT D10-100
MUTU	K-400

KOLOM LEVEL	K3-1
LANTAI 2	
LANTAI 1	
DIMENSI	300 x 300
TULANGAN UTAMA	8 D13
SENGKANG	D10-100
MUTU	K-300

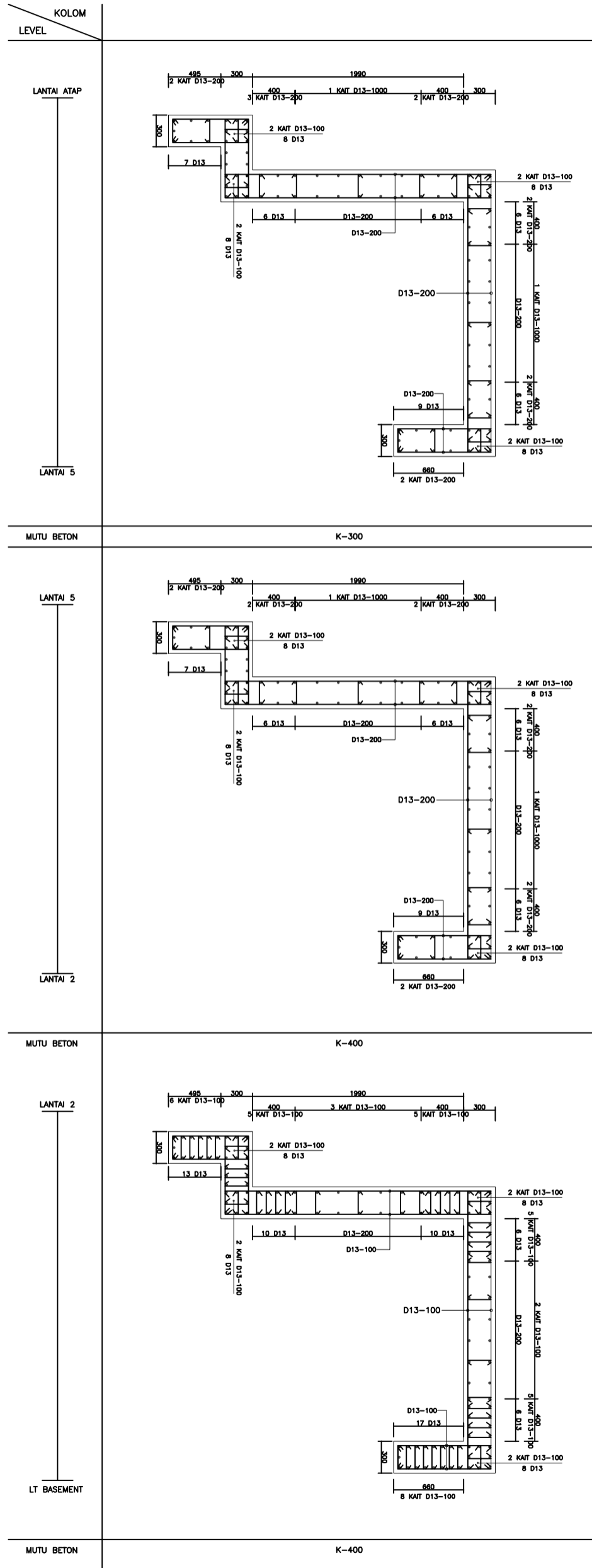
LANTAI 5	
BASEMENT	
DIMENSI	400 x 800
TULANGAN UTAMA	18 D16
SENGKANG	D10-100 + 2 KAPT D10-100
MUTU	K-400

KOLOM LEVEL	K7-1
LANTAI 1	
BASEMENT	
DIMENSI	400 x 400
TULANGAN UTAMA	8 D16
SENGKANG	D10-100
MUTU	K-400

KOLOM	SW.2
LEVEL	
LANTAI ATAP	
LANTAI 5	
MUTU BETON	K-300
LANTAI 5	
LANTAI 2	
MUTU BETON	K-400
LANTAI 2	
LT BASEMENT	
MUTU BETON	K-400

KOLOM	SW.1 & SW.4
LEVEL	
LANTAI ATAP	
LANTAI 5	
MUTU BETON	K-300
LANTAI 5	
LANTAI 2	
MUTU BETON	K-400
LANTAI 2	
LT BASEMENT	
MUTU BETON	K-400

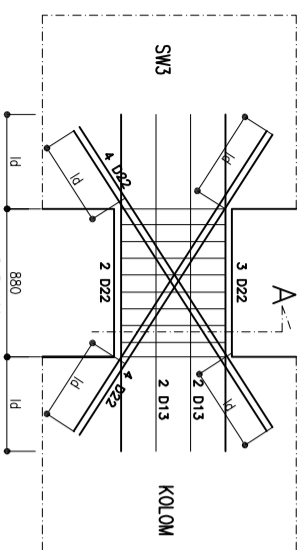




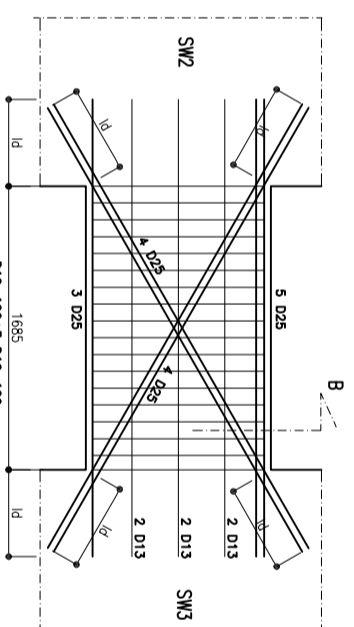
Tipe Balok	G1-1					G1-2					G1-3					G1-4					G1-5				
Posisi	Tumpuan	Lapangan	Tumpuan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Lapangan		
Dimensi	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700		
Tulangan Atas	8 D16	5 D16	4 D16	4 D16	4 D16	5 D16	5 D16	5 D16	5 D16	6 D16	6 D16	5 D16	4 D16	4 D16	4 D16	4 D16	4 D16	4 D16	4 D16	4 D16	4 D16	4 D16	4 D16		
Tulangan Samping	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10		
Tulangan Bawah	8 D16	5 D16	4 D16	4 D16	4 D16	4 D16	4 D16	4 D16	4 D16	6 D16	4 D16	4 D16	4 D16	4 D16	4 D16	4 D16	4 D16	4 D16	4 D16	4 D16	4 D16	4 D16	4 D16		
Senkang	3 D10-100	3 D10-100	3 D10-100	3 D10-100	3 D10-100	3 D10-200	3 D10-200	3 D10-100	3 D10-100	3 D10-100	3 D10-100	3 D10-100	3 D10-100	3 D10-100	3 D10-200	3 D10-100	3 D10-100	3 D10-100	3 D10-100	3 D10-100	3 D10-100	3 D10-100	3 D10-100		

Tipe Balok	G1-6					G1-7					G1-8					G1-9					G1-10				
Posisi	Tumpuan	Lapangan	Tumpuan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Lapangan		
Dimensi	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700		
Tulangan Atas	6 D22	2 D22	3 D22	3 D22	2 D22	2 D22	2 D22	2 D22	2 D22	4 D22	2 D10	2 D10	2 D10	7 D25	5 D25	3 D25	3 D25	3 D25	3 D25	3 D25	3 D25	3 D25	3 D25		
Tulangan Samping	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10		
Tulangan Bawah	3 D22	3 D22	2 D22	2 D22	2 D22	2 D22	2 D22	2 D22	2 D22	3 D22	4 D25	4 D25	4 D25	4 D25	3 D25	3 D25	3 D25	3 D25	3 D25	3 D25	3 D25	3 D25	3 D25		
Senkang	D10-100	D10-100	D10-100	D10-100	D10-100	D10-200	D10-200	D10-100	D10-100	D10-200	3 D10-100	3 D10-100	3 D10-100	3 D10-100	3 D10-100	3 D10-100	3 D10-100	3 D10-100	3 D10-100	3 D10-100	3 D10-100	3 D10-100	3 D10-100		

Tipe Balok	G1-11					G1-12					G1-13					G1-15							
Posisi	Tumpuan	Lapangan	Tumpuan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Lapangan	
Dimensi	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	
Tulangan Atas	6 D16	4 D16	8 D22	8 D22	3 D22	4 D22	4 D22	5 D22	2 D22	4 D22	4 D22	4 D22	4 D22	4 D22	4 D22	4 D22	4 D22	4 D22	4 D22	4 D22	4 D22	4 D22	3 D22
Tulangan Samping	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10
Tulangan Bawah	4 D16	4 D16	4 D22	4 D22	4 D22	4 D22	4 D22	3 D22	3 D22	2 D22	3 D22	3 D22	3 D22	3 D22	3 D22	3 D22	3 D22	3 D22	3 D22	3 D22	3 D22	3 D22	3 D22
Senkang	D10-100	D10-200	D10-100	D10-100	D10-200	D10-100	D10-100	D10-100	D10-100	D10-200	D10-100	D10-100	D10-100	D10-100	D10-100	D10-100	D10-100	D10-100	D10-100	D10-100	D10-100	D10-100	D10-150



POTONGAN		A
Dimensi	300 x 700	
Tulangan Atas	3 D22	
Tulangan Samping	4 D13	
Tulangan Bawah	2 D22	
Senkang	D10-100	



POTONGAN		B
Dimensi	300 x 1000	
Tulangan Atas	5 D25	
Tulangan Samping	6 D13	
Tulangan Bawah	3 D25	
Senkang	D13-100	

TIPE BALOK	G2-1		TUMPUAN	TUMPUAN	G2-2		TUMPUAN	TUMPUAN	G2-3		TUMPUAN	TUMPUAN	G2-3A		TUMPUAN	TUMPUAN	G2-4		TUMPUAN	TUMPUAN	G2-5	
	TUMPUAN	LAPANGAN			LAPANGAN	LAPANGAN			LAPANGAN	LAPANGAN			LAPANGAN	LAPANGAN			LAPANGAN	LAPANGAN			LAPANGAN	LAPANGAN
DIMENSI	300 x 600	300 x 600	300 x 600	300 x 600	300 x 600	300 x 600	300 x 600	300 x 600	300 x 600	300 x 600	300 x 600	300 x 600	300 x 600	300 x 600	300 x 600	300 x 600	300 x 600	300 x 600	300 x 600	300 x 600	300 x 600	300 x 600
TULANGAN ATAS	3 D22	3 D22	3 D22	3 D16	3 D16	3 D16	4 D16	3 D16	3 D16	3 D16	2 D22	2 D22	2 D22	2 D22	2 D22	2 D22	4 D19	2 D19	3 D19	3 D19	3 D19	
TULANGAN SAMPING	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10
TULANGAN BAWAH	3 D22	3 D22	3 D22	3 D16	3 D16	3 D16	3 D16	3 D16	3 D16	3 D16	2 D22	2 D22	2 D22	2 D22	2 D22	2 D22	2 D19	3 D19	3 D19	3 D19	2 D19	2 D19
SENGKANG	3 D10-100	3 D10-100	3 D10-100	D10-100	D10-100	D10-100	D10-100	D10-100	D10-100	D10-150	D10-100	D10-100	D10-150	D10-100	D10-100	D10-100	D10-150	D10-150	D10-150	D10-150	D10-150	D10-150

TIPE BALOK	G2-6		G3-1		TUMPUAN	LAPANGAN	TUMPUAN	LAPANGAN	G3-2		TUMPUAN	TUMPUAN	G3-2A		TUMPUAN	LAPANGAN	G3-2B		TUMPUAN	TUMPUAN	G3-3	
	TUMPUAN	LAPANGAN	TUMPUAN	LAPANGAN					LAPANGAN	LAPANGAN			LAPANGAN	LAPANGAN			LAPANGAN	LAPANGAN			LAPANGAN	LAPANGAN
DIMENSI	300 x 600	300 x 600	300 x 500	300 x 500	300 x 500	300 x 500	300 x 500	300 x 500	300 x 500	300 x 500	300 x 500	300 x 500	300 x 500	300 x 500	300 x 500	300 x 500	300 x 500	300 x 500	300 x 500	300 x 500	300 x 500	300 x 500
TULANGAN ATAS	4 D19	2 D19	3 D16	3 D16	3 D16	3 D16	3 D16	4 D16	3 D16	3 D16	3 D16	4 D16	3 D16	3 D16	3 D16	3 D16	7 D16	2 D10	3 D16	3 D16	3 D16	3 D16
TULANGAN SAMPING	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10
TULANGAN BAWAH	2 D19	3 D19	3 D16	3 D16	3 D16	3 D16	3 D16	3 D16	3 D16	3 D16	3 D16	3 D16	3 D16	3 D16	3 D16	3 D16	4 D16	4 D16	3 D16	3 D16	3 D16	5 D16
SENGKANG	D10-150	D10-200	D10-100	D10-200	3 D10-100	3 D10-100	3 D10-100	3 D10-100	3 D10-100	D10-100	D10-200	D10-100	D10-100	D10-100	D10-100	D10-100	D10-100	D10-100	D10-100	D10-100	D10-100	D10-200

TIPE BALOK	G7-1		G7-2		G8-1		G8-2		G8-3		G9-1	
	TUMPUAN	LAPANGAN	TUMPUAN	LAPANGAN	TUMPUAN	LAPANGAN	TUMPUAN	LAPANGAN	TUMPUAN	LAPANGAN	TUMPUAN	LAPANGAN
DIMENSI	400 x 700	400 x 700	400 x 700	400 x 700	250 x 400	250 x 400	250 x 400	250 x 400	250 x 400	250 x 400	250 x 600	250 x 600
TULANGAN ATAS	9 D22	3 D22	6 D22	3 D22	5 D16	2 D16	5 D16	2 D16	2 D16	2 D16	5 D16	3 D16
TULANGAN SAMPING	2 D10	2 D10	2 D10	2 D10	-	-	-	-	-	-	2 D10	2 D10
TULANGAN BAWAH	3 D22	6 D22	3 D22	5 D22	3 D16	3 D16	3 D16	3 D16	3 D16	3 D16	3 D16	4 D16
SENGKANG	D10-100	D10-200	D10-150	D10-200	D10-100	D10-200	D10-100	D10-200	D10-150	D10-100	D10-100	D10-200



TIPE BALOK	B4-4		B5-1		B5-2		B6-1		B6-2		B8-1		B8-2									
	TUMPUAN	LAPANGAN	TUMPUAN	TUMPUAN	TUMPUAN	LAPANGAN	TUMPUAN	LAPANGAN	TUMPUAN	LAPANGAN	TUMPUAN	LAPANGAN	TUMPUAN	LAPANGAN								
DIMENSI	250 x 500	250 x 500	250 x 500	200 x 400	200 x 400	200 x 400	200 x 400	200 x 400	200 x 400	150 x 400	150 x 400	150 x 400	150 x 400	150 x 400	250 x 400	250 x 400	250 x 400	250 x 400	250 x 400	250 x 400	250 x 400	
TULANGAN ATAS	4 D16	2 D16	2 D16	2 D16	2 D16	3 D16	2 D16	2 D13	2 D13	4 D13	2 D13	4 D13	2 D13	2 D13	4 D16	2 D16	4 D16	2 D16	4 D16	3 D16	2 D16	
TULANGAN SAMPING	2 D10	2 D10	2 D10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
TULANGAN BAWAH	2 D16	2 D16	2 D16	2 D16	2 D16	2 D16	2 D16	2 D16	2 D16	2 D13	2 D13	2 D13	2 D13	2 D13	3 D16	2 D16	2 D16	3 D16	2 D16	3 D16	2 D16	
SEKANGKANG	D10-200	D10-200	D10-200	D10-200	D10-200	D10-200	D10-200	D10-200	D10-200	D10-200	D10-200	D10-200	D10-200	D10-200	D10-200	D10-200	D10-100	D10-100	D10-100	D10-100	D10-100	D10-100

TIPE BALOK	B8-3		B8-4		B8-5		B9-1	
	TUMPUAN	LAPANGAN	TUMPUAN	LAPANGAN	TUMPUAN	LAPANGAN	TUMPUAN	LAPANGAN
DIMENSI	250 x 400	250 x 400	250 x 400	250 x 400	250 x 400	250 x 400	250 x 600	250 x 600
TULANGAN ATAS	3 D16	2 D16	3 D16	2 D16	2 D16	2 D16	4 D16	3 D16
TULANGAN SAMPING	-	-	-	-	-	-	2 D10	2 D10
TULANGAN BAWAH	2 D16	4 D16	3 D16	5 D16	2 D16	3 D16	4 D16	3 D16
SEKANGKANG	D10-200	D10-200	D10-200	D10-200	D10-200	D10-200	D10-150	D10-150

Tipe Balok	CL1-1		CL1-2		CL1-3		CL2-1		CL2-2		CL2-3		CL4-1	
Posisi	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Lapangan
Dimensi	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 700	300 x 600	300 x 600	300 x 600	300 x 600	300 x 600	300 x 600	250 x 500	250 x 500
Tulangan Atas	8 D22	4 D22	5 D22	3 D22	8 D16	4 D16	7 D22	4 D22	4 D22	2 D22	5 D22	3 D22	2 D16	2 D16
Tulangan Samping	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10	2 D10
Tulangan Bawah	4 D22	4 D22	3 D22	3 D22	4 D16	4 D16	3 D22	3 D22	2 D22	2 D22	2 D22	2 D22	2 D16	2 D16
Sengkang	D10-100	D10-200	D10-100	D10-200	D10-100	D10-200	D10-100	D10-200	D10-100	D10-200	D10-100	D10-200	D10-200	D10-200

Tipe Balok	CL8-1		CL8-2		CL11-1		CL11-2	
Posisi	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Lapangan	Tumpuan	Lapangan
Dimensi	250 x 400	250 x 400	250 x 400	250 x 400	300 x 800	300 x 800	300 x 800	300 x 800
Tulangan Atas	3 D16	3 D16	6 D16	3 D16	6 D16	4 D16	4 D16	4 D16
Tulangan Samping	-	-	-	-	2 D10	2 D10	2 D10	2 D10
Tulangan Bawah	3 D16	3 D16	3 D16	3 D16	4 D16	4 D16	4 D16	4 D16
Sengkang	D10-100	D10-200	D10-100	D10-200	D10-100	D10-200	D10-100	D10-200